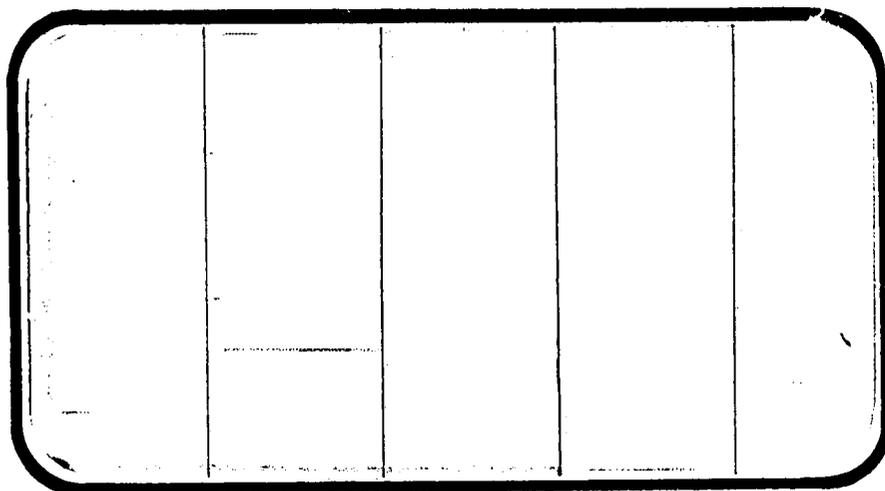




NATIONAL AERONAUTICS AND SPACE ADMINISTRATION

NASA CR:

134415



(NASA-CR-134415) RESULTS OF REACTION CONTROL SYSTEM ON-ORBIT JET SIMULATION USING AN 0.0175-SCALE CONFIGURATION 3 SPACE SHUTTLE ORBITER MODEL (21-0) IN (Chrysler Corp.) 56 p HC \$4.25 CSCL 21H

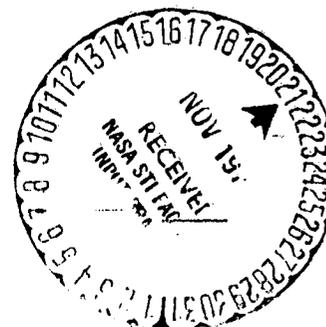
N75-10170

Unclas

G3/20 53180

SPACE SHUTTLE

AEROTHERMODYNAMIC DATA REPORT



JOHNSON SPACE CENTER

HOUSTON, TEXAS

DATA MANAGEMENT services.

SPACE DIVISION



CHRYSLER CORPORATION

N75-10170

DATE: APRIL, 1975

24-53180

# PUBLICATION CHANGE

THE FOLLOWING CHANGES APPLY TO PUBLICATION: DMS-DR-2172

TITLE: RESULTS OF REACTION CONTROL SYSTEM ON-ORBIT JET SIMULATION USING AN 0.0175-SCALE CONFIGURATION 3 SPACE SHUTTLE ORBITER MODEL (21-0) IN THE LaRC 60-FOOT VACUUM SPHERE (0A99)

NUMBER: DMS-DR-2172 DATE: OCTOBER 1974 BRANCH: FLIGHT TECHNOLOGY

Table V, p. 27 lists the following data:

Run #	Configuration	Impingement Forces (Lbs) Side
5	-139 Orbiter (MOD) LT. Pitch-up	
6	-139 Orbiter (MOD) LT. Pitch-up	-.1768

Corrected data are as follows:

Run #	Configuration	Impingement Forces (Lbs) Side
5	-139 Orbiter (MOD) LT. Pitch-down	
6	-139 Orbiter (MOD) LT. Pitch-down	.1768

Prepared by: Operations--Maurice Moser Jr.

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PAGE 1 OF 1

DISTRIBUTION SAME AS FOR  
ABOVE PUBLICATION

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SPACE DIVISION  CHRYSLER CORPORATION

October, 1974

DMS-DR-2172  
NASA-CR-134,415

RESULTS OF REACTION CONTROL SYSTEM  
ON-ORBIT JET SIMULATION USING AN 0.0175-SCALE  
CONFIGURATION 3 SPACE SHUTTLE ORBITER MODEL (21-0)  
IN THE LaRC 60-FOOT VACUUM SPHERE (OA99)

By

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Prepared under NASA Contract Number NAS9-13247

By

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Chrysler Corporation Space Division  
New Orleans, La. 70189

for

Engineering Analysis Division

Johnson Space Center  
National Aeronautics and Space Administration  
Houston, Texas

WIND TUNNEL TEST SPECIFICS:

Test Number: 60-foot Vacuum Sphere R3289  
NASA Series Number: OA99  
Model Number: 21-0  
Test Dates: March 26-April 12, 1974  
Occupancy Hours: 52

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Chrysler Corporation Space Division assumes no responsibility for the data presented other than display characteristics.

RESULTS OF REACTION CONTROL SYSTEM  
ON-ORBIT JET SIMULATION USING AN O.0175-SYSTEM  
CONFIGURATION 3 SPACE SHUTTLE ORBITER MODEL (21-0)  
IN THE LaRC 60-FOOT VACUUM SPHERE (OA99)

By J. Marroquin, Rockwell International Space Division

ABSTRACT

An experimental investigation was conducted in the Langley Research Center 60-foot Vacuum Sphere (test OA99) from March 26 through April 12, 1974, to obtain detailed effects of the RCS jet flow direct impingement on the Orbiter during on-orbit flight of the Space Shuttle Vehicle.

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## INTRODUCTION

An experimental investigation was conducted March 26 through April 12, 1974, to determine RCS direct impingement effects on the Space Shuttle Vehicle during on-orbit flight. Langley Research Center 60-foot Vacuum Sphere was the test site; Orbiter Model 21-0 was used. Nominal test conditions are in Table I. —

RCS flow was simulated by blowing a jet of cold air from non-metric nozzles attached to the model sting support system near the fuselage base (figure 2d). Thrust was obtained by setting the nozzle plenum pressure (as specified by the nozzle calibration). Nozzle thrust was measured by a 10 lb. capacity load cell. Nozzles were calibrated at near vacuum conditions and corrected to total vacuum conditions. A plot of both measured and theoretical thrusts as a function of model plenum pressure is in figure 2i.

Three RCS on-orbit flight conditions were simulated. Six-component force data were measured on the complete model using the LaRC 0.50-inch diameter balance (number HH09). It was supported by a LaRC sting.

Six force data runs, including three re-runs, were recorded at various sphere pressure levels and displayed on oscillograph recorders. Model pressure data, applicable to several altitudes, were obtained for two RCS modes using a dummy sting.

Two pressure hook-ups were used. One hook-up, used during tests of pitch down jets ( $N_{70}$ ), measured pressures on the wing, bodyflap, SSME, and fuselage (see Table IVa). The other hook-up, used during tests of pitch-up jets ( $N_{69}$ ), measured pressures on the vertical tail (see Table IVb).

NOMENCLATURE  
général

<u>Symbol</u>	<u>Plot Symbol</u>	<u>Definition</u>
$\delta_{BF}$	BDFLAP	bodyflap deflection angle, degrees
$\delta_e$	ELEVTR	elevator deflection angle, degrees
$\delta_{RF}$	RUDFLR	rudder flare angle, degrees
$\alpha$	ALPHA	angle of attack, degrees
$\beta$	BETA	angle of sideslip, degrees
$P_a$		atmospheric pressure, psia

Reference and C. G. Definitions

$b_{ref}$	BREF	wing span or reference span, ft
$L_{ref}$	LREF	reference length or wing mean aerodynamic chord, ft
$S_{ref}$	SREF	wing area or reference area, ft <sup>2</sup>
MRC	MRC	moment reference center
C.G.		center of gravity

Body-Axis System

N	NF	normal force, lbs
A	AF	axial force, lbs
Y	SE	side force, lbs
m	PM	pitching moment, in-lbs
n	YM	yawing moment, in-lbs
l	RM	rolling moment, in-lbs

NOMENCLATURE (Concluded)  
 Additional Nomenclature

<u>Symbol</u>	<u>Plot Symbol</u>	<u>Definition</u>
$P_c$		model RCS plenum chamber pressure, psia
$P_{V1}$		sphere pressure prior to run, microns
$P_{V2}$		sphere pressure after run, microns
$T_c$		model plenum chamber temperature, °F
$T_V$		sphere chamber temperature, °F

Simulation Nozzle Design

$A^*$		nozzle throat area, in <sup>2</sup>
$A_{ref}$		reference area, in <sup>2</sup>
$e$		exit
$\dot{m}$		mass flow rate of the nozzle, lbm/sec
$TH$		vacuum thrust of the nozzle, lbf
$\gamma$		specific heat
$e$		expansion ratio
$\theta_p$		nozzle lip angle
$\lambda$		plume shape parameter
$\phi$		Newtonian impact angle

Abbreviations

RCS	reaction control system
SSME	space shuttle main engines
OMS	orbiter maneuvering system
MPS	main propulsion system
L/H	left hand side
R/H	right hand side

CONFIGURATION INVESTIGATED\_\_\_\_\_

The test article (provided by Rockwell) was an 0.0175-scale model (21-0) of the VL70-000139 definition of the SSV Orbiter Configuration 3. The model was constructed of light weight, glazed cast foam with fixed control surfaces. A three-view drawing of the model showing the principal dimensions and photographs of the model installed in the chamber are shown in figures 2a and 3a, respectively.

The model was installed vertically in the LaRC 60-foot Vacuum Chamber. The RCS plenum-nozzle assembly was non-metrically attached to the sting. Nozzle N<sub>68</sub> (yaw control) and N<sub>70</sub> (pitch down control) was located on the left side of the RCS plenum. Nozzle N<sub>69</sub> (pitch up control) was located on the plenum right side. Each nozzle contained two orifices, through which cold air flowed, as shown in figure 2e. Orifices were plugged on non-firing nozzles.

The following nomenclature was used to designate the model components:

O = B<sub>17</sub> C<sub>7</sub> E<sub>22</sub> F<sub>5</sub> M<sub>6</sub> N<sub>39</sub> R<sub>5</sub> V<sub>5</sub> W<sub>103</sub>

<u>Component</u>	<u>Definition</u>
B <sub>17</sub>	Vehicle configuration 3 fuselage lightweight Orbiter per Rockwell lines VL70-000139.
C <sub>7</sub>	Basic vehicle configuration 3 canopy per Rockwell lines VL70-000139
E <sub>22</sub>	Basic vehicle configuration 3 elevon per W <sub>103</sub> Rockwell lines VL70-000139
F <sub>5</sub>	Basic vehicle body flap 3 configuration per Rockwell lines VL70-000139
M <sub>6</sub>	Modified OMS-RCS pod for the Rockwell SSV configuration 3 (VL70-000139)

- |  |  |  |  |  |  |  |
|--|--|--|--|--|--|--|
|  |  |  |  |  |  |  |
|--|--|--|--|--|--|--|
- N<sub>39</sub> Configuration 3A MPS nozzles
- R<sub>5</sub> Basic vehicle 3 configuration rudder per Rockwell lines VL70-000095
- V<sub>5</sub> Basic vehicle configuration 3 light weight Orbiter. Center-line vertical tail doublewedge airfoil with rounded leading edge. VL70-000139 and VL70-000095
- W<sub>103</sub> Vehicle configuration 3 wing per lines VL70-000139 (same planform as W<sub>89</sub> except dihedral at IE).

RCS Nozzles

- N<sub>68</sub> L/H yaw nozzle, not canted
- N<sub>69</sub> R/H pitch up, not canted
- N<sub>70</sub> L/H pitch down, canted 12° AFT and 20° outboard

## RCS NOZZLE DESIGN

The simulation technique employed for the nozzle design was based on the analytical method of Hill and Draper, in which a single unique parameter,  $\lambda$ , was derived that closely approximates the internal iso-properties of a vacuum plume. The correlation between test and full-scale flight forces, moments, and pressures is summarized below.

	full scale	model
<b>A. RCS Jet Characteristics</b>		
Chamber Pressure, $P_c$	150 psia	1000 psia
Chamber Temperature, $T_c$	5450°R	530 °R
Specific Heat, $\gamma$	1.232	1.4
Nozzle Throat Area $A^*$	3.619 in. <sup>2</sup>	0.0011045 in. <sup>2</sup>
Expansion Ratio, $\epsilon$	20	6.2
Nozzle Lip Angle, $\theta_p$	9°	10°
Exit Area, $A_e$	72.382 in. <sup>2</sup>	0.00685 in. <sup>2</sup>
Exit Mach No., $M_e$	3.93	3.4
Mass Flow Rate, $\dot{m}$	3.287 lbm/sec	0.0242 lbm/sec
Vacuum Thrust, TH	950 lbf.	1.78 lbf.
<b>B. Simulation Parameter</b>		
Plume Parameter, $\lambda$	4.74	4.74 (matched)
Throat Area Ratio ( $A^*/A_{ref}$ )	3.619	3.619 (matched)
Total pressure Ratio ( $P_c/P_A$ )	$5.47 \times 10^9$	$5.45 \times 10^7$ (close)

## RCS NOZZLE CALIBRATION

The RCS nozzles were calibrated in the intermittent blowdown-vacuum test section 7' x 5' x 16' Test Chamber Rocket Nozzle Test Facility at the Los Angeles Division from 13 through 15 March 1974. The calibration determined nozzle thrust as a function of plenum chamber pressure ( $P_c$ ).

Test chamber and nozzle plenum chamber pressures were recorded by a dial gage. Nozzle thrust was measured by a Revere No. 244267, 10-lb capacity load cell. All three nozzles were calibrated under near vacuum conditions to simulate the same on-orbit flight conditions tested in the LRC vacuum sphere; see Table I. Calibration results are shown in figure 2i.

## TEST FACILITY DESCRIPTION

The 60-foot Vacuum Sphere at Langley Research Center, Hampton, Virginia is shown in figure 3. This cell is capable of simulating pressure altitudes over 91.5 Km. (300,000 ft.). Evacuation is continuously maintained by six oil diffusion pumps.

Test OA99 data were recorded within 570 milliseconds after RCS jets commenced firing to maintain adequate pressure altitude. A high speed electronically operated, hydraulically controlled valve (located outside and under the test chamber) was used to control RCS jet flow. The valve was operated with hydraulic pressures between 450 psia and 1000 psia.

Vacuum chamber initial pressure, final pressure, and nominal temperature are presented in Table I for each run.

## DATA REDUCTION

Force and moments measured by the Orbiter internal strain-gauge balance were reduced about the MRC  $X_0 = 1076.68$ ,  $Z_0 = 375.0$ , and  $Y_0 = 0.0$  (Table V).

Pressure data were obtained on three oscillograph recorders and hand reduced (Table VI).

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Rockwell Drawing VL70-000095, Lines Control Vertical Tail, Configuration 139.  
  
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TABLE I. - Test Conditions

DATE	RUN NO.	NOZZLE CONF.	RCS PLENUM		VACUUM SPHERE			PROGRAM TEST TIME (MILLI-SECONDS)	REMARKS
			P <sub>c</sub> PSIA	T <sub>c</sub> °F	T <sub>v</sub> °F	PV <sub>1</sub> MICRON HG	PV <sub>2</sub> MICRON HG		
4-3-74	1	N68	1000	100	90	4.3	10.0	570	FORCE & MOMENT DATA
4-3-74	2	N68	↕	99	90	6.5	21.0	↕	↕
4-4-74	3	N69	↕	88	93	2.3	22.0	↕	↕
4-4-74	4	N69	1000	88	93	22.0	30.0	570	FORCE & MOMENT DATA
4-5-74	5	N70	750	97	82	0.61	15.0	570	FORCE & MOMENT DATA
4-5-74	6	N70	↕	97	82	9.0	22.0	↕	↕
4-10-74	7	N70	1000	83	76	31.3	47.5	150	PRESS. DATA PITCH-DOWN(SPH LEAKAGE)
4-10-74	8	↕	400	83	76	41.9	49.4	150	PRESS. DATA PITCH-DOWN(SPH LEAKAGE)
4-11-74	9	↕	1000	80	78	5.3	20.0	570	REPEAT OF PITCH-DOWN
↕	10	↕	↕	80	78	19.2	34.9	↕	↕
↕	11	↕	↕	79	77	32.1	47.4	↕	↕
4-11-74	12	N70	↕	79	77	46.0	61.0	↕	↕
4-12-74	13	N69	↕	104	85	0.41	14.0	↕	↕
↕	14	↕	↕	104	85	11.4	25.3	↕	↕
↕	15	↕	↕	104	85	23.3	38.2	↕	↕
↕	16	↕	↕	104	85	36.2	51.2	↕	↕
4-12-74	17	N69	1000	104	85	48.6	63.6	570	PITCH-UP

TABLE II.

RCS VACUUM DIRECT IMPINGEMENT TEST

TEST: 0699		DATA SET/RUN NUMBER COLLATION SUMMARY											DATE: 4-14-74		
DATA SET IDENTIFIER	CONFIGURATION	SCHD.		$\delta_e$	$\delta_{BF}$	$\delta_{RF}$	$P_a$	$P_c$	$T_c$	$T_c$	RCS FIRING	NO. OF RUNS	DATE	TEST RUN NUMBER	
		$\alpha$	$\beta$												
1	0 + N68	0	0	0	0	0	0	1000	100		YAW (LEFT)	1	FORCE	4-3-74	
2	0 + N68	▲	▲	▲	▲	▲	▲	1000	99		YAW (LEFT)	1	▲	4-3-74	
3	0 + N69							1000	88		PITCH UP (R/H)	1		4-4-74	
4	0 + N69							1000	88		PITCH UP (R/H)	1		4-4-74	
5	0 + N70							1000	97		PITCH DOWN (L/H)	1	▼	4-5-74	
6	0 + N70							750	97		PITCH DOWN (L/H)	1	FORCE	4-5-74	
7	0 + N70							1000	83		PITCH DOWN (L/H)		PRESS	4-10-74	
8	0 + N70							450	83		PITCH DOWN (L/H)		▲	4-10-74	
9	0 + N70							1000	80		RERUN PITCH DN L/H		▲	4-11-74	
10	0 + N70							▲	80				▲		
11	0 + N70							▼	79				▼		
12	0 + N70							1000	79		RERUN PITCH DN (L/H)			4-11-74	
13	0 + N69							1000	104		PITCH UP (R/H)			4-12-74	
14	0 + N69							▲					▲		
15								▲					▲		
16		▲	▲	▲	▲	▲	▲	▲					▲		
17	0 + N69	0	0	0	0	0	0	1000	104		PITCH UP (R/H)		PRESS	4-12-74	

7 13 19 25 31 37 43 49 55

0 = P17C7E22F16N39R55M103

α OR β

SCHEDULES

COEFFICIENTS

TABLE III. - MODEL DIMENSIONAL DATA

MODEL COMPONENT : BODY - B<sub>17</sub>  
 GENERAL DESCRIPTION : Fuselage, 3 configuration, lightweight orbiter  
per Rockwell Lines VL70-000139  
 \_\_\_\_\_  
 MODEL SCALE: 0.0175  
 \_\_\_\_\_  
 DRAWING NUMBER : VL70-000139

DIMENSIONS :	FULL SCALE	MODEL SCALE
Length = In.	<u>1290.3</u>	<u>22.58025</u>
Max Width - In.	<u>267.6</u>	<u>4.6830</u>
Max Depth - In.	<u>244.5</u>	<u>4.27875</u>
Fineness Ratio	<u>4.82175</u>	<u>4.82175</u>
Area - Ft <sup>2</sup>	<u>386.67</u>	<u>0.118398</u>
Max. Cross-Sectional	_____	_____
Planform	_____	_____
Wetted	_____	_____
Base	_____	_____

\*REVISED 4/24/74

TABLE III. - MODEL DIMENSIONAL DATA - Continued.

MODEL COMPONENT : CANOPY - C7

GENERAL DESCRIPTION : Configuration 3 per Rockwell Lines VL70-000139

MODEL SCALE: 0.0175

DRAWING NUMBER : VL70-000139

DIMENSIONS :	FULL SCALE	MODEL SCALE
*Length ( $X_0=433$ to $X_0=578$ ) IN.FS	<u>145.00</u>	<u>2.538</u>
Max Width	<u>57.14</u>	<u>9.99950</u>
Max Depth	<u>          </u>	<u>          </u>
Fineness Ratio	<u>          </u>	<u>          </u>
Area	<u>          </u>	<u>          </u>
Max. Cross-Sectional	<u>          </u>	<u>          </u>
Planform	<u>          </u>	<u>          </u>
Wetted	<u>          </u>	<u>          </u>
Base	<u>          </u>	<u>          </u>

TABLE III. - MODEL DIMENSIONAL DATA - Continued.

MODEL COMPONENT: ELEVON - E22

GENERAL DESCRIPTION: 3 Configuration per W103 Rockwell Lines

VL70-000139 data for (1) of (2) sides.

MODEL SCALE: 0.0175

DRAWING NUMBER: VL70-000139

<u>DIMENSIONS:</u>	<u>FULL-SCALE</u>	<u>MODEL SCALE</u>
Area - Ft <sup>2</sup>	<u>205.52</u>	<u>0.06293</u>
Span (equivalent) - In.	<u>353.34</u>	<u>6.18345</u>
Inb'd equivalent chord	<u>114.78</u>	<u>2.00855</u>
Outb'd equivalent chord	<u>55.00</u>	<u>0.9625</u>
Ratio movable surface chord/ total surface chord		
At Inb'd equiv. chord	<u>0.208</u>	<u>0.208</u>
At Outb'd equiv. chord	<u>0.400</u>	<u>0.400</u>
Sweep Back Angles, degrees		
Leading Edge	<u>0.00</u>	<u>0.00</u>
Trailing Edge	<u>- 10.24</u>	<u>- 10.24</u>
Hingeline	<u>0.00</u>	<u>0.00</u>
Area Moment (Normal to hinge line) Ft <sup>3</sup>	<u>1548.07</u>	<u>0.00820</u>

TABLE III. - MODEL DIMENSIONAL DATA - Continued.

MODEL COMPONENT : BODY FLAP - F<sub>5</sub>

GENERAL DESCRIPTION : Body flap for Fuselage B<sub>17</sub>, 3 configuration  
per Rockwell Lines VL70-000139.

MODEL SCALE: 0.0175

DRAWING NUMBER : VL70-000139

DIMENSIONS :	FULL SCALE	MODEL SCALE
Length - In.	<u>84.70</u>	<u>1.48225</u>
Max Width - In.	<u>267.6</u>	<u>4.6830</u>
Max Depth	<u>          </u>	<u>          </u>
Fineness Ratio	<u>          </u>	<u>          </u>
Area - Ft <sup>2</sup>	<u>          </u>	<u>          </u>
Max. Cross-Sectional	<u>142.5195</u>	<u>0.04364</u>
Planform	<u>          </u>	<u>          </u>
Wetted	<u>          </u>	<u>          </u>
Base	<u>38.0958</u>	<u>0.01167</u>

TABLE III. - MODEL DIMENSIONAL DATA - Continued.

MODEL COMPONENT : OMS POD - M<sub>0</sub>

GENERAL DESCRIPTION: Configuration 3

Aft end of OMS POD cut off for RCS installation. See Figures 2 and 3  
and Convair Model Drawing No. WT-73-108150.

MODEL SCALE: 0.0175

DRAWING NUMBER : VL70-000139

DIMENSIONS :	FULL SCALE	MODEL SCALE
Length (OMS Fwd. Sta $X_0=1233.0$ )	<u>327.000</u>	<u>5.7225</u>
Max Width (@ $X_0 = 1450.0$ )	<u>109.000</u>	<u>1.9075</u>
Max Depth	<u>          </u>	<u>          </u>
Fineness Ratio	<u>          </u>	<u>          </u>
Area	<u>          </u>	<u>          </u>
Max. Cross-Sectional	<u>          </u>	<u>          </u>
Planform	<u>          </u>	<u>          </u>
Wetted	<u>          </u>	<u>          </u>
Base	<u>          </u>	<u>          </u>

TABLE III. - MODEL DIMENSIONAL DATA - Continued.

MODEL COMPONENT: M32 NOZZLES - M39

GENERAL DESCRIPTION: Configuration 34 MP3 Nozzles

MODEL SCALE = 0.0175

DRAWING NO. See figures.

<u>DIMENSIONS</u>	<u>FULL SCALE</u>	<u>MODEL SCALE</u>
Mach No. _____		
Length ~ in.		
Gimbal Point to Exit Plane _____	_____	_____
Throat to Exit Plane _____	_____	_____
Diameter ~ in.		
Exit _____	<u>94.000</u>	<u>1.645</u>
Throat _____	_____	_____
Inlet _____	_____	_____
Area ~ ft. <sup>2</sup> .		
Exit _____	<u>48.193</u>	<u>0.01475669</u>
Throat _____	_____	_____
Gimbal Point (station) ~ in.		
Upper Nozzle		
X _____		
Y _____		
Z _____		
NOT USED		
Lower Nozzles		
X _____	<u>.1462.0</u>	<u>25.585</u>
Y _____	<u>+ 53.000</u>	<u>+ 0.9275</u>
Z _____	<u>342.7</u>	<u>5.99725</u>
Null Position ~ deg.		
Upper Nozzle		
Pitch _____	_____	_____
Yaw _____	_____	_____
Lower Nozzles		
Pitch _____	_____	_____
Yaw _____	_____	_____

\*REVISED 4/24/74

TABLE III. - MODEL DIMENSIONAL DATA - Continued.

MODEL COMPONENT: RUDDER - R<sub>5</sub>

GENERAL DESCRIPTION: 2A, 3 and 3A Configuration per Rockwell Lines  
VL70-000095

MODEL SCALE: 0.0175

DRAWING NUMBER: VL70-000095

<u>DIMENSIONS:</u>	<u>FULL-SCALE</u>	<u>MODEL SCALE</u>
*Area - Ft <sup>2</sup>	<u>100.15</u>	<u>0.031</u>
Span (equivalent) - In.	<u>201.0</u>	<u>3.5175</u>
Inb'd equivalent chord	<u>91.585</u>	<u>1.60274</u>
Outb'd equivalent chord	<u>50.833</u>	<u>0.88958</u>
Ratio movable surface chord/ total surface chord		
At Inb'd equiv. chord	<u>0.400</u>	<u>0.400</u>
At Outb'd equiv. chord	<u>0.400</u>	<u>0.400</u>
Sweep Back Angles, degrees		
Leading Edge	<u>34.83</u>	<u>34.83</u>
Trailing Edge	<u>26.25</u>	<u>26.25</u>
Hingeline	<u>34.83</u>	<u>34.83</u>
* Area Moment (Product of Area & $\bar{c}$ ) - Ft <sup>3</sup>	<u>526.13</u>	<u>0.00279</u>
*Product of Area and Mean Chord Inc.	<u>73.2</u>	<u>1.281</u>

TABLE III. - MODEL DIMENSIONAL DATA - Continued.

MODEL COMPONENT: VERTICAL - V<sub>5</sub>

GENERAL DESCRIPTION: Centerline Vertical Tail, doublewedge airfoil with rounded leading edge.

MODEL SCALE: 0.0175

DRAWING NUMBER: VL70-000139, VL70-000095

<u>DIMENSIONS:</u>	<u>FULL-SCALE</u>	<u>MODEL SCALE</u>
<u>TOTAL DATA</u>		
Area (Theo) - Ft <sup>2</sup>		
Planform	<u>425.92</u>	<u>0.13042</u>
Span (Theo) - In	<u>315.72</u>	<u>5.52510</u>
Aspect Ratio	<u>1.675</u>	<u>1.675</u>
Rate of Taper	<u>0.507</u>	<u>0.507</u>
Taper Ratio	<u>0.404</u>	<u>0.404</u>
Sweep Back Angles, degrees		
Leading Edge	<u>45.000</u>	<u>45.000</u>
Trailing Edge	<u>26.249</u>	<u>26.249</u>
0.25 Element Line	<u>47.130</u>	<u>47.130</u>
Chords:		
Root (Theo) WP	<u>268.50</u>	<u>4.69875</u>
Tip (Theo) WP	<u>108.47</u>	<u>1.89823</u>
MAC	<u>199.81</u>	<u>3.49667</u>
Fus. Sta. of .25 MAC	<u>1463.50</u>	<u>25.61125</u>
W. P. of .25 MAC	<u>635.522</u>	<u>11.1216</u>
B. L. of .25 MAC	<u>0.00</u>	<u>0.00</u>
Airfoil Section		
Leading Wedge Angle - Deg	<u>10.000</u>	<u>10.000</u>
Trailing Wedge Angle - Deg	<u>14.290</u>	<u>14.290</u>
Leading Edge Radius	<u>2.00</u>	<u>0.0350</u>
Void Area	<u>13.17</u>	<u>0.23048</u>
Blanketed Area	<u>12.67</u>	<u>0.22173</u>

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TABLE III. - MODEL DIMENSIONAL DATA - Concluded.

MODEL COMPONENT: <u>WING-W 103</u>	
GENERAL DESCRIPTION: <u>Configuration 3 Orbiter per Lines VL70-000139.</u>	
MODEL SCALE: <u>0.0175</u>	
TEST NO.	DWG. NO. <u>VL70-000139</u>
DIMENSIONS:	FULL-SCALE      MODEL SCALE
<b>TOTAL DATA</b>	
Area (Theo.) - Ft <sup>2</sup>	
Planform	<u>2690.00</u> <u>0.0823813</u>
Span (Theo) In.	<u>936.68</u> <u>16.3919</u>
Aspect Ratio	<u>2.265</u> <u>2.265</u>
Rate of Taper	<u>1.177</u> <u>1.177</u>
Taper Ratio	<u>0.200</u> <u>0.200</u>
Dihedral Angle, degrees	<u>3.500</u> <u>3.500</u>
Incidence Angle, degrees	<u>3.000</u> <u>3.000</u>
Aerodynamic Twist, degrees	<u>+ 3.000</u> <u>+ 3.000</u>
Sweep Back Angles, degrees	
Lead Edge	<u>45.000</u> <u>45.000</u>
Trail Edge	<u>- 10.24</u> <u>- 10.24</u>
0.25 Element Line	<u>35.209</u> <u>35.209</u>
<b>Chords:</b>	
Root (Theo) B.P.O.O.	<u>689.24</u> <u>12.0617</u>
Tip, (Theo) B.P.	<u>137.85</u> <u>2.41237</u>
MAC	<u>474.81</u> <u>8.309175</u>
Fus. Sta. of .25 MAC	<u>1136.89</u> <u>19.895575</u>
W.P. of .25 MAC	<u>299.20</u> <u>5.236</u>
B.L. of .25 MAC	<u>182.13</u> <u>3.187275</u>
<b>EXPOSED DATA</b>	
Area (Theo) - Ft <sup>2</sup>	<u>1752.29</u> <u>0.536551</u>
Span, (Theo) - In. BP108	<u>720.68</u> <u>12.6119</u>
Aspect Ratio	<u>2.058</u> <u>2.058</u>
Taper Ratio	<u>0.2451</u> <u>0.2451</u>
<b>Chords</b>	
Root BP108	<u>562.40</u> <u>9.842</u>
Tip 1.00 $\frac{b}{2}$	<u>137.85</u> <u>2.412375</u>
MAC	<u>393.03</u> <u>6.87803</u>
Fus. Sta. of .25 MAC	<u>1185.31</u> <u>20.74293</u>
W.P. of .25 MAC	<u>300.20</u> <u>5.2535</u>
B.L. of .25 MAC	<u>251.76</u> <u>4.4058</u>
<b>Airfoil Section (Rockwell Mod NASA)</b> XXXX-64	
Root $\frac{b}{2}$ =	<u>0.10</u> <u>0.10</u>
Tip $\frac{b}{2}$ =	<u>0.12</u> <u>0.12</u>
<b>Data for (1) of (2) Sides</b>	
Leading Edge Cuff	<u>120.33</u> <u>0.236845</u>
Planform Area - Ft <sup>2</sup>	<u>560.0</u> <u>9.8000</u>
Leading Edge Intersects Fus M. L. @ Sta	<u>1035.0</u> <u>18.1125</u>
Leading Edge Intersects Wing @ Sta	

TABLE IV. - Instrumentation and Transducer Information  
a. (N70) Pitch-Down

PRESS. TAP LOCATION	TAP NO.	RECORDER		TRANSDUCER			REMARKS
		RECORDER CHANNEL	INV. NO.	S/N	EXCIT.	RANGE	
L/H WING	1	3	88634	5574	10 V.	1.0	RUNS 7 & 8 RECORDER PROBLEMS RUNS 9, 10, 11 & 12
	2	3	89021	5570	↕	1.0	
	3	3	138027	2203	↕	0.5	
	4	3	NA	5499	↕	1.0	
	5	3	100882	6225	↕	↕	
	6	3	130688	1866	↕	1.0	
	7	3	130686	2346	↕	0.5	
	8	3	138031	2207	↕	1.0	
	9	3	130678	1856	↕	↕	
	10	3	130677	1855	↕	↕	
L/H WING BODY FLAP	11	3	130689	1867	↕	↕	
	12	2	87550	5489	↕	↕	
	13	2	100984	6226	↕	↕	
	14	2	87469	5496	↕	↕	
	15	2	89220	5497	↕	↕	
	16	2	85396	5249	↕	↕	
	17	2	87827	5522	↕	↕	
	18	2	85398	5251	↕	↕	
	19	2	88238	5577	10 V	1.0	
	20	1	125941	12922	5 V.	1.0	
BODY FLAP L/H FUSELAGE	21	1	125939	12920	10 V	3.0	
	22	1	130692	1890	10 V	1.0	
	23	1	88239	5579	↕	↕	
	24	1	87472	5503	↕	↕	
	25	1	87552	5491	↕	1.0	
	26	1	96863	6073	↕	0.5	
	27	3	138026	2202	↕	↕	
	28	3	138029	2205	↕	↕	
	29	3	138032	2208	↕	↕	
	30	3	138034	2210	↕	↕	
L/H FUSELAGE SSME SSME SSME PLENUM CHAMBER	31	3	138033	2209	↕	0.5	
	32	3	138035	2211	↕	0.5	
	33	3	138028	2204	↕	1.0	
	34	2	101501	6110	↕	1.0	
	35	2	100877	6228	↕	1.0	
	Pc	3	86210	5253	10 V	1.0	

TABLE IV. - Instrumentation and Transducer Information - Concluded.  
 b. (N69) Pitch-Up

PRESS. TAP LOCATIONS	TAP NO.	RECORDER		TRANSDUCER			REMARKS
		RECORDER	CHANNEL	INV. NO.	S/N	EXCIT RANGE	
VERTICAL ↑	36	3	7	138027	2203	10 V	0.5
	37	3	17	138031	2207	↑	0.5
	38	3	25	138026	2202		0.5
	39	3	11	100882	6225		1.0
	40	3	13	130688	1866		1.0
	41	3	15	130686	2346		1.0
	42	3	27	138029	2205		0.5
	43	3	29	138032	2208		0.5
	44	3	19	130678	1856		1.0
	45	3	21	130677	1855		1.0
	46	3	23	130689	1867		1.0
	47	3	31	138034	2210		0.5
	48	3	33	138033	2209		0.5
	49	3	35	138035	2211		0.5
	50	3	37	138028	2204		10 V
VERTICAL PLENUM CHAMBER	P <sub>c</sub>	3	26	---	---		---

TABLE V. - RCS DIRECT IMPINGEMENT FORCE DATA

Run #	Configuration	Plenum Pressure	Impingement Normal	Impingement Axial	Impingement Side	Impingement Pitch	Impingement Roll	Moments (in-lbs) Yaw
1	-139 Orbiter(MOD) Left Yaw Noz.	1000(psi)	-.0562	-.0083	-.0052	.3454	-.3497	.1033
2	-139 Orbiter(MOD) Left Yaw Noz.	1000(psi)	-.0459	-.0035	-.0077	.3226	-.3338	.1214
3	-139 Orbiter(MOD) RT. Pitch-up	1000(psi)	.0019	-.1116	-.2634	-.1716	-1.3367	2.1386
4	-139 Orbiter(MOD) RT. Pitch-up	1000(psi)	-.0032	-.1089	-.2599	-.1916	-1.3235	2.1011
5	-139 Orbiter(MOD) LT. Pitch-down	1000(psi)	-.9491	-.5081	.1803	7.8420	-1.9005	-1.1690
6	-139 Orbiter(MOD) LT. Pitch-down	800(psi)	-.7710	-.4209	.1768	6.4115	-1.5331	-.9325

TABLE VI. RCS DIRECT IMPINGEMENT PRESSURE DATA

RCS Jet Group: Right side, Up-firing

Run 13

Tap #      Imp. Press. ~ P<sub>I</sub> MMHg

P<sub>C</sub> = 1000 Psia

36.	0.65
37	1.25
38	2.10
39	2.60
40	1.70
41	0.15
42	0.50
43	0.85
44	1.45
45	1.95
46	1.80
47	0.10
48	0.75
49	1.40
50	1.25

RCS Jet Group: Left side, Down-firing

Run 9

Tap #      P<sub>I</sub> ~ MMHg

Tap #      P<sub>I</sub> ~ MMHg

Tap #      P<sub>I</sub> ~ MMHg

1	0	13	0.
2.	0	14	.1
3	.1	15	.7
4	.1	16	8.3
5	.1	17	1.9
6	.1	18	.2
7	.1	19	0
8	.1	20	27.0
9	.4	21	110.0
10	.5	22	3.0
11	.6	23	38.0
12	.2	24	8.0

25	13.0
26	.2
27	.5
28	.1
29	0.
30	.2
31	.1
32	0.
33	.5
34	.8
35	.3

**Notes**

1. Positive directions of force coefficients, moment coefficients, and angles are indicated by arrows
2. For clarity, origins of wind and stability axes have been displaced from the center of gravity

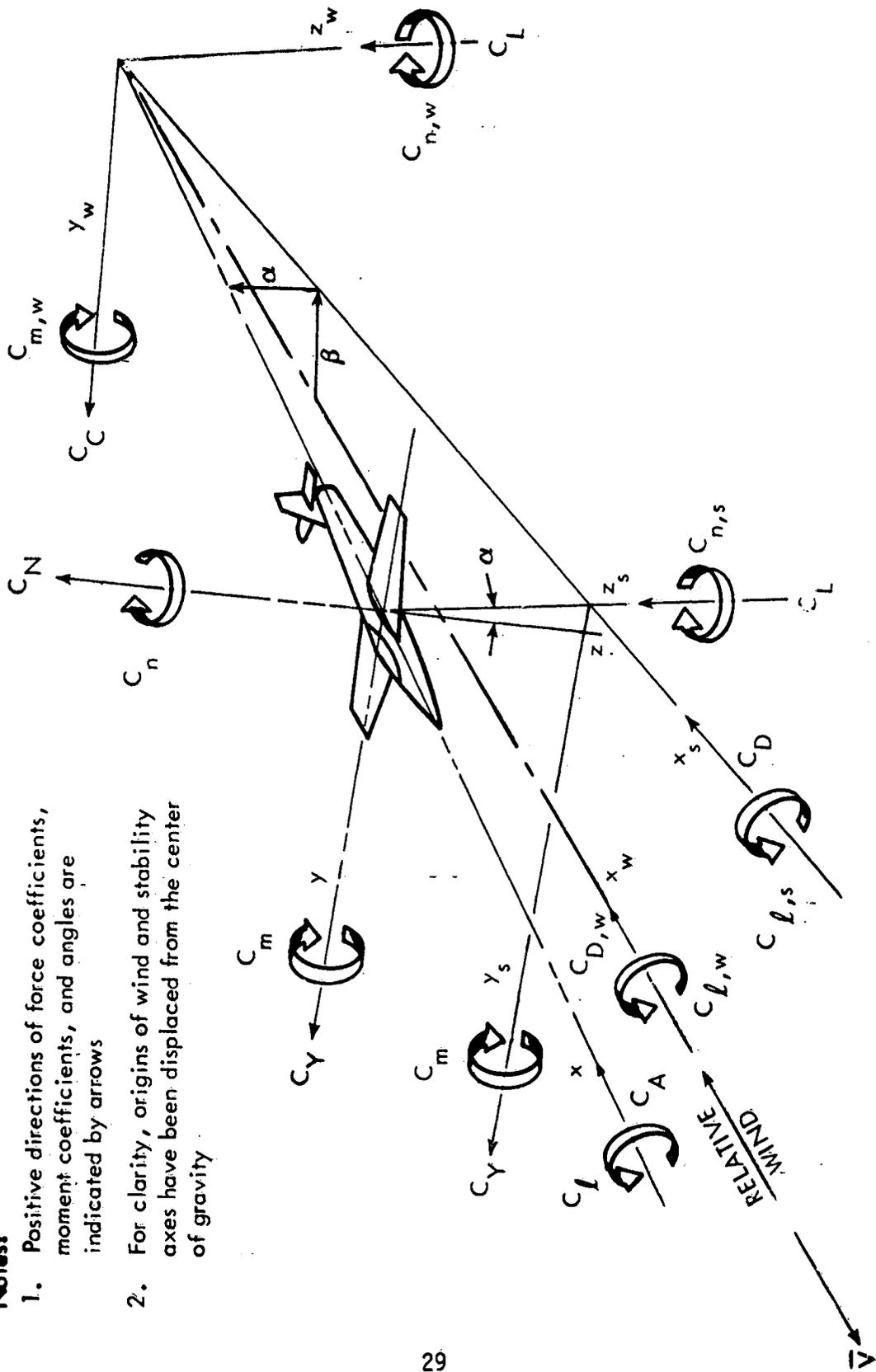
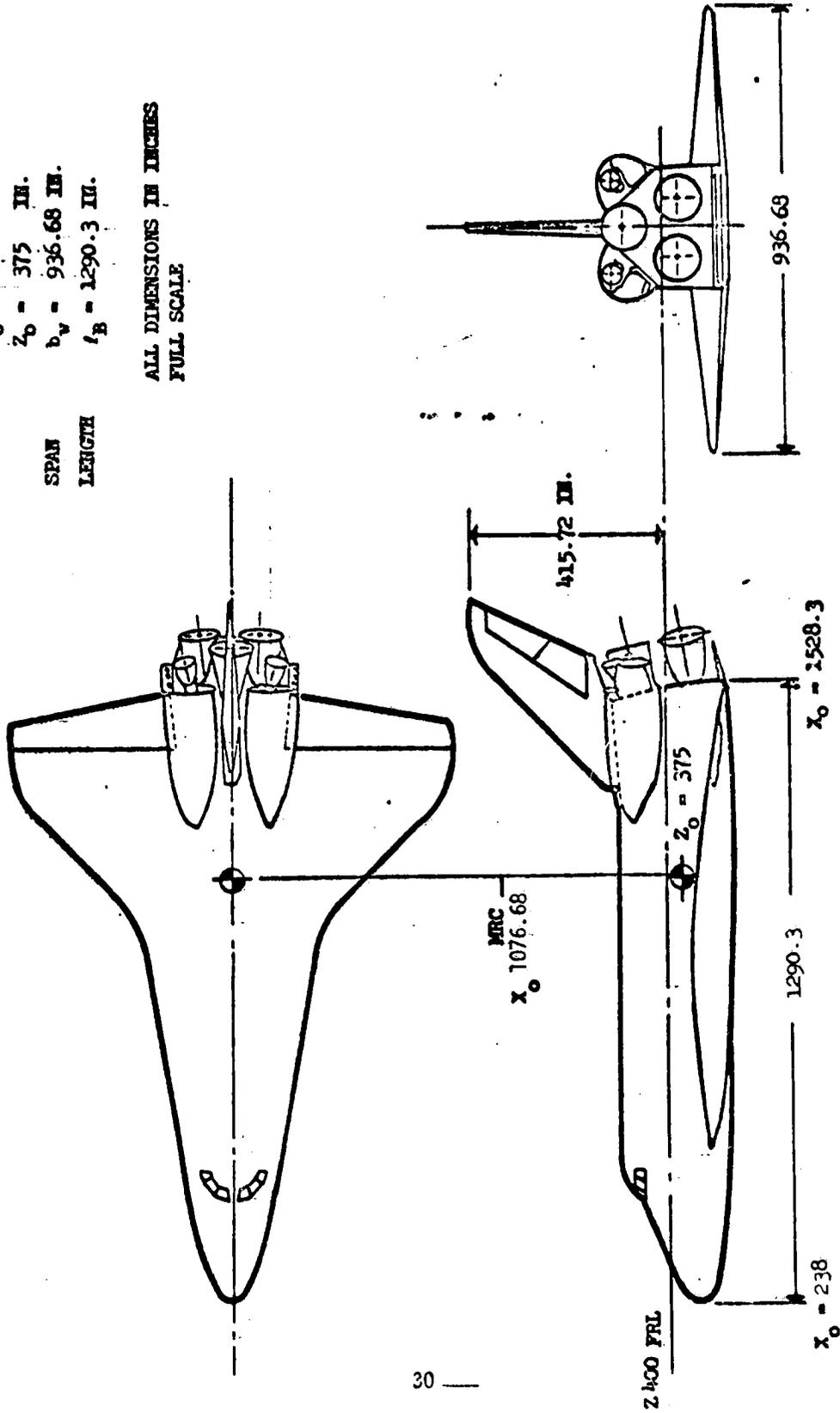


Figure 1. - Axis Systems

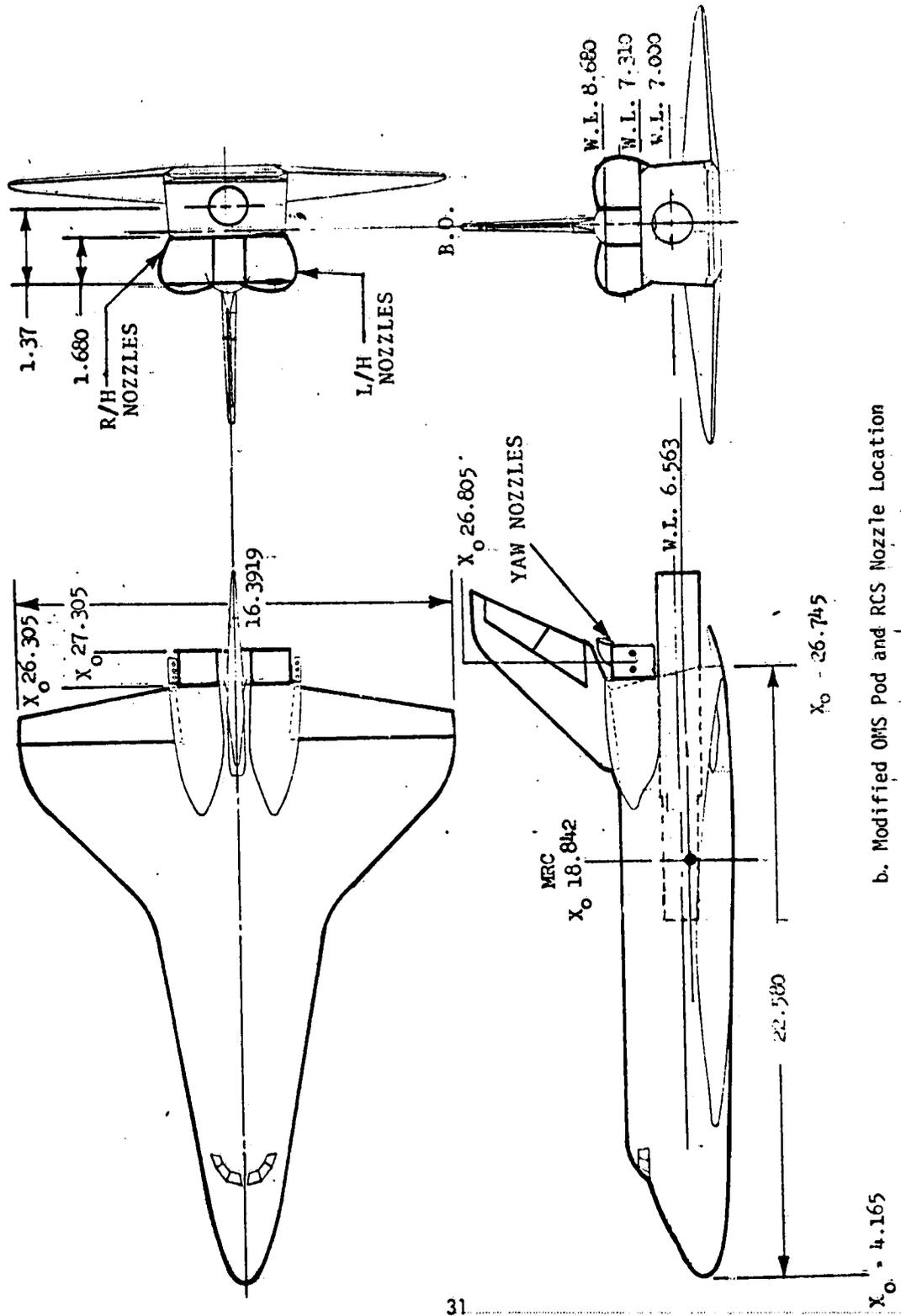
REFERENCE	DIMENSIONS (FS)
AREA	$S_v = 2690 \text{ FT}^2$
MAC	$C = 474.8 \text{ IN.}$
C.O.	$X_0 = 1076.48 \text{ IN.}$
SPAN	$Z_0 = 375 \text{ IN.}$
LENGTH	$b_v = 936.68 \text{ IN.}$
	$l_B = 1290.3 \text{ IN.}$

ALL DIMENSIONS IN INCHES  
FULL SCALE

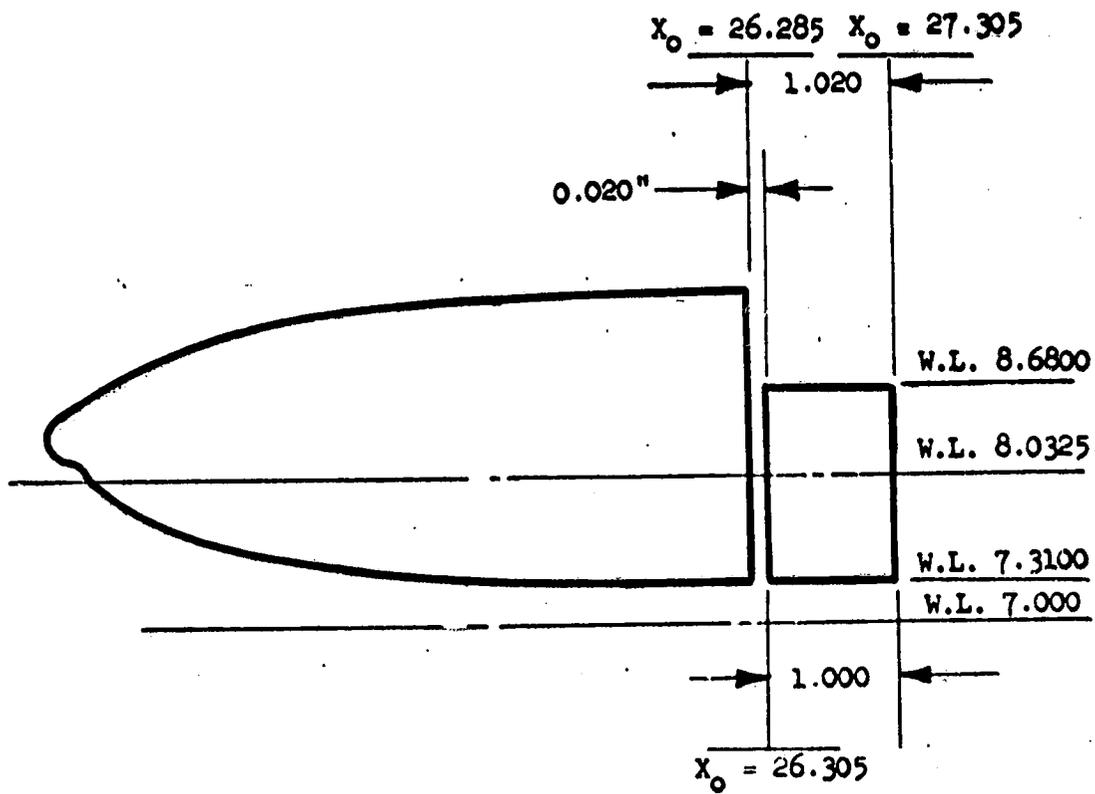


a. General Model Arrangement

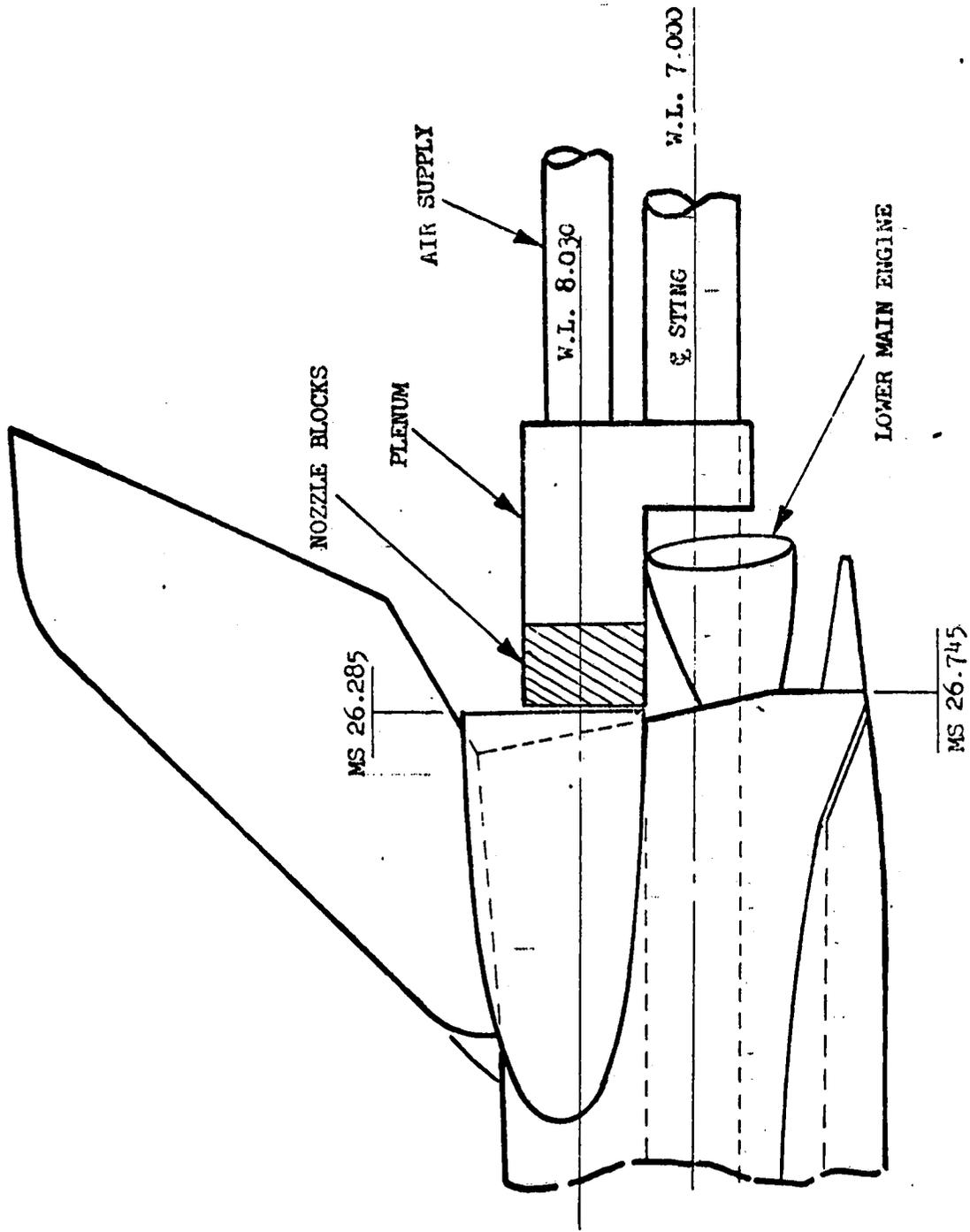
Figure 2. - Model information.



b. Modified OMS Pod and RCS Nozzle Location  
Figure 2. - Continued.



c. M<sub>6</sub> OMS Pod  
 Figure 2. - Continued.

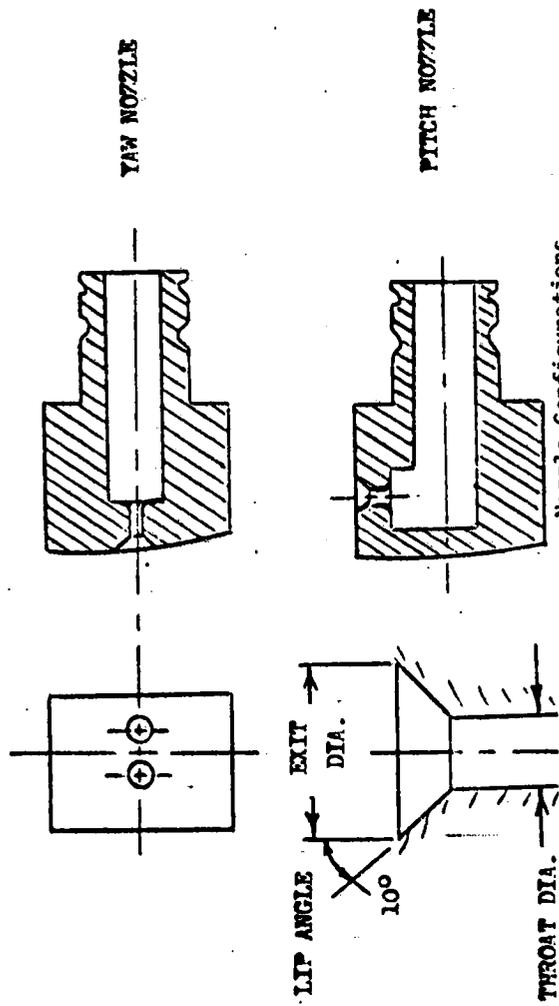


d. RCS Plenum Nozzle Block Installation

Figure 2. - Continued.

NOZZLE GEOMETRY

NOZZLE NO.	DASH NO.	NO. OF NOZZLE	THROAT		EXIT		AREA RATIO $\left(\frac{A_e}{A_t}\right)$	NOTES
			DIA. (IN.)	AREA (IN. <sup>2</sup> )	DIA. (IN.)	AREA (IN. <sup>2</sup> )		
N68	- 5	2	0.0375	.001104	0.0934	.006850	6.2	YAW JET. NOT CANTED LEFT HAND SIDE.
N69	- 7	2	0.0375	.001104	0.0934	.006850	6.2	PITCH UP, RIGHT HAND SIDE. NOT CANTED
N70	- 6	2	0.0375	.001104	0.0934	.006850	6.2	PITCH DOWN, LEFT HAND SIDE CANTED 12° AFT & 20° OUTBOARD
			LIP ANGLE $\theta_p = 10^\circ$					

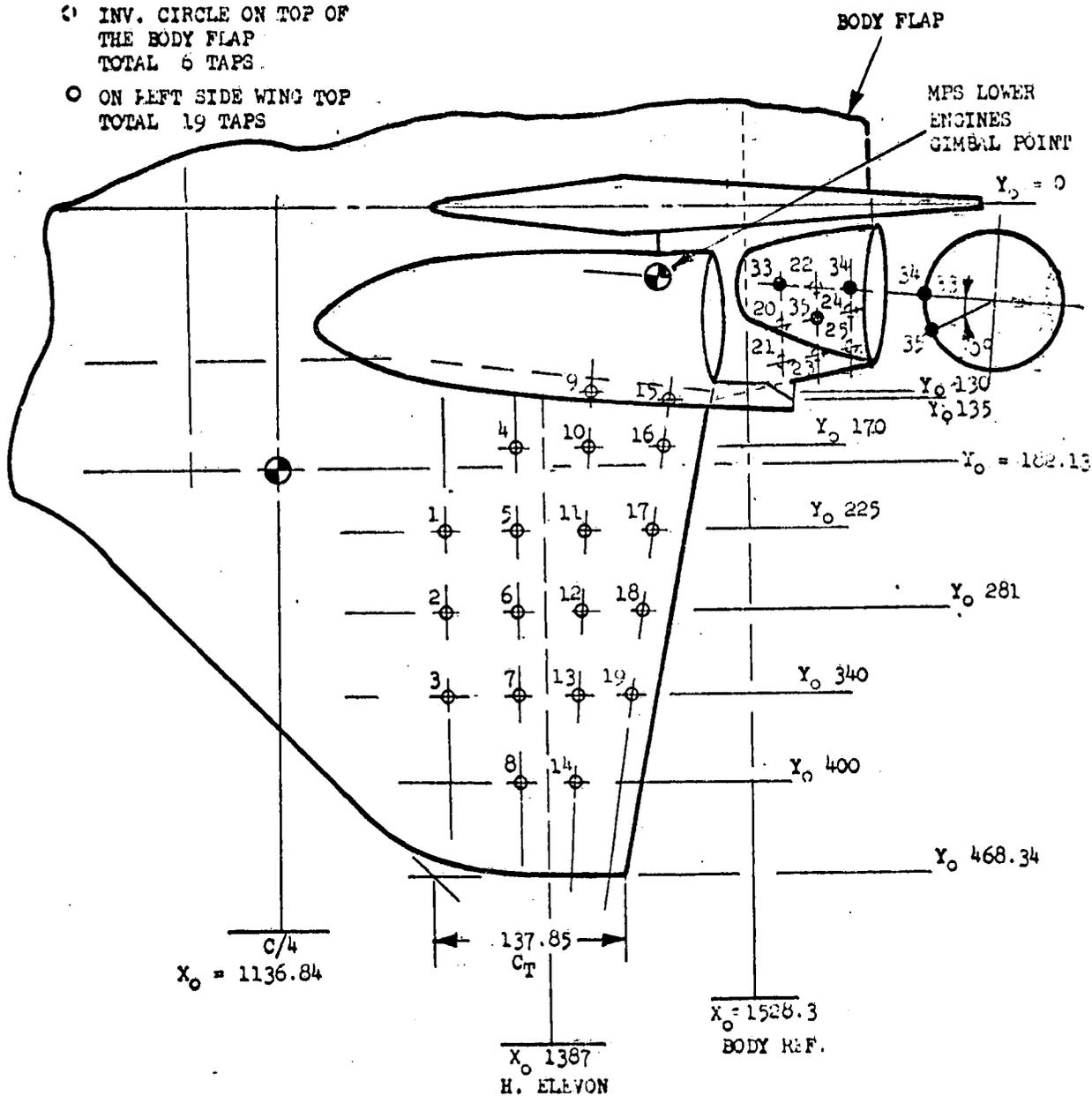


e. Nozzle Configurations

Figure 2. - Continued.

LEGEND:

- DARK CIRCLE AT CGME, NOZZLE BELL TOP & ONE OUT AND DOWN 30° TOTAL - 3 TAPS
- INV. CIRCLE ON TOP OF THE BODY FLAP TOTAL 6 TAPS
- ON LEFT SIDE WING TOP TOTAL 19 TAPS



f. L/H Wing, Body Flap and SSME Nozzle Pressure Tap Location/Identification.

Figure 2. - Continued.

L/H WING SURFACE PRESSURE TAPS (19)

<u>TAP NO.</u>	<u>X<sub>0</sub></u>	<u>Y<sub>0</sub></u>	<u>LOCATION</u>
1	1320	225	(19) PRESSURE TAPS LOCATED ON THE UPPER L/H WING SURFACE  
2	1320	281	
3	1320	340	
4	1370	170	
5	1370	225	
6	1370	281	
7	1370	340	
8	1370	400	
9	1424	130	
10	1420	170	
11	1418	225	
12	1414	281	
13	1412	340	
14	1408	400	
15	1478	135	
16	1472	170	
17	1466	225	
18	1456	281	
19	1448	340	

f. Pressure Tap Locations  
Figure 2. - Continued.

BODY FLAP PRESSURE TAPS (6)

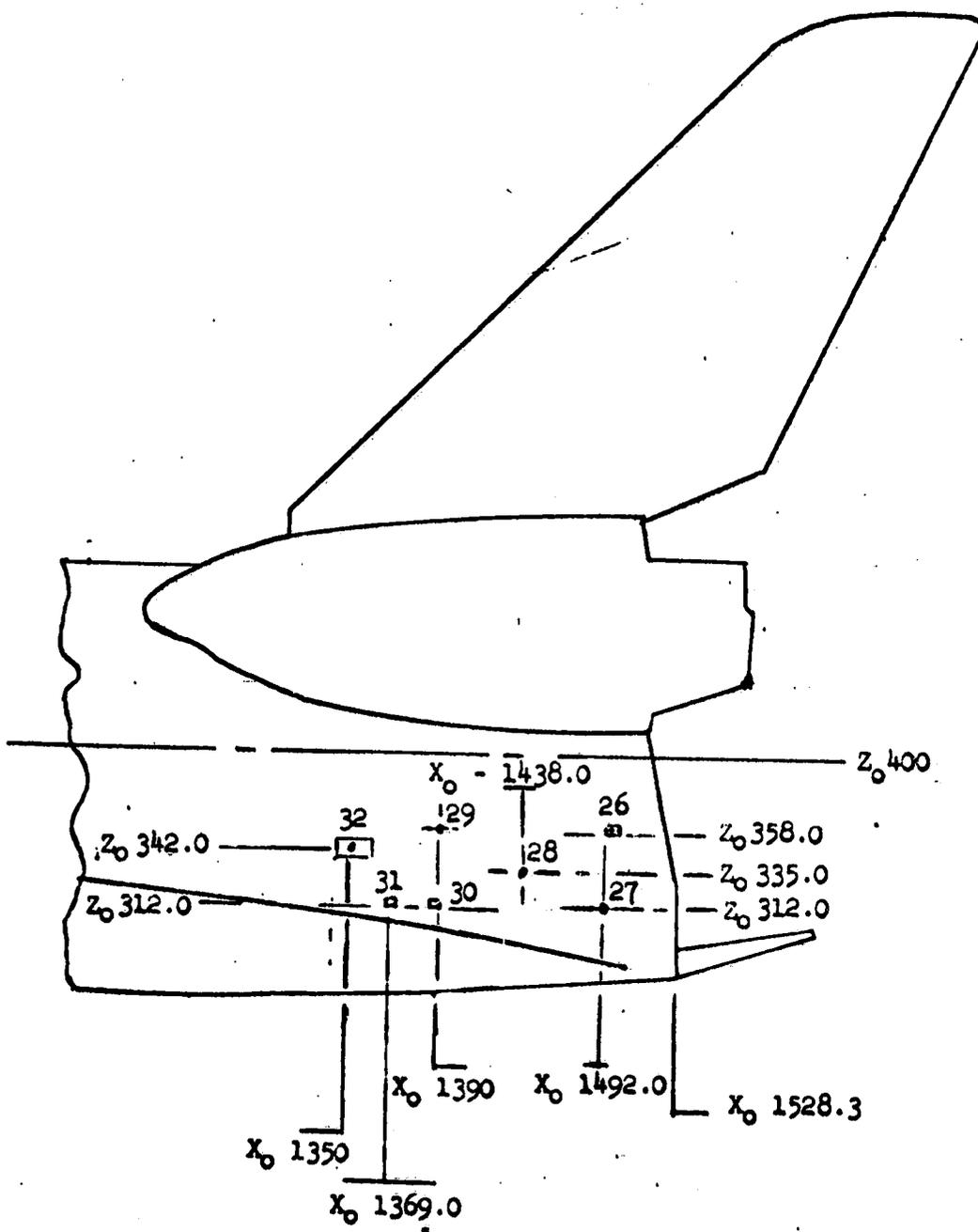
TAP NO.	X <sub>o</sub>	Y <sub>o</sub>	LOCATION
20	1556	85	(6) PRESSURE TAPS LOCATED ON THE UPPER L/H SIDE OF BODY FLAP
21	1556	112	
22	1582	58	
23	1582	106	
24	1604	75	
25	1604	100	(6) PRESSURE TAPS LOCATED ON THE UPPER L/H SIDE OF BODY FLAP

SSME NOZZLE BELL PRESSURE TAPS (3)

TAP NO.	X <sub>o</sub>	Y <sub>o</sub>	LOCATION
33	1556	☒ THRUST	FWD UPPER CENTERLINE OF THRUST OF SSME NOZZLE BALL.
34	1604	☒ THRUST	AFT UPPER CENTERLINE OF THRUST OF SSME NOZZLE BALL.
35	1582	30° OFF CENTER	LEFT HAND SIDE OF SSME NOZZLE BELL LOOKING FWD, 30° CCW FROM CENTERLINE OF THRUST

Pressure Tap Locations.

Figure 2f. - Concluded.



g. L/H Lower Aft Fuselage Pressure Taps

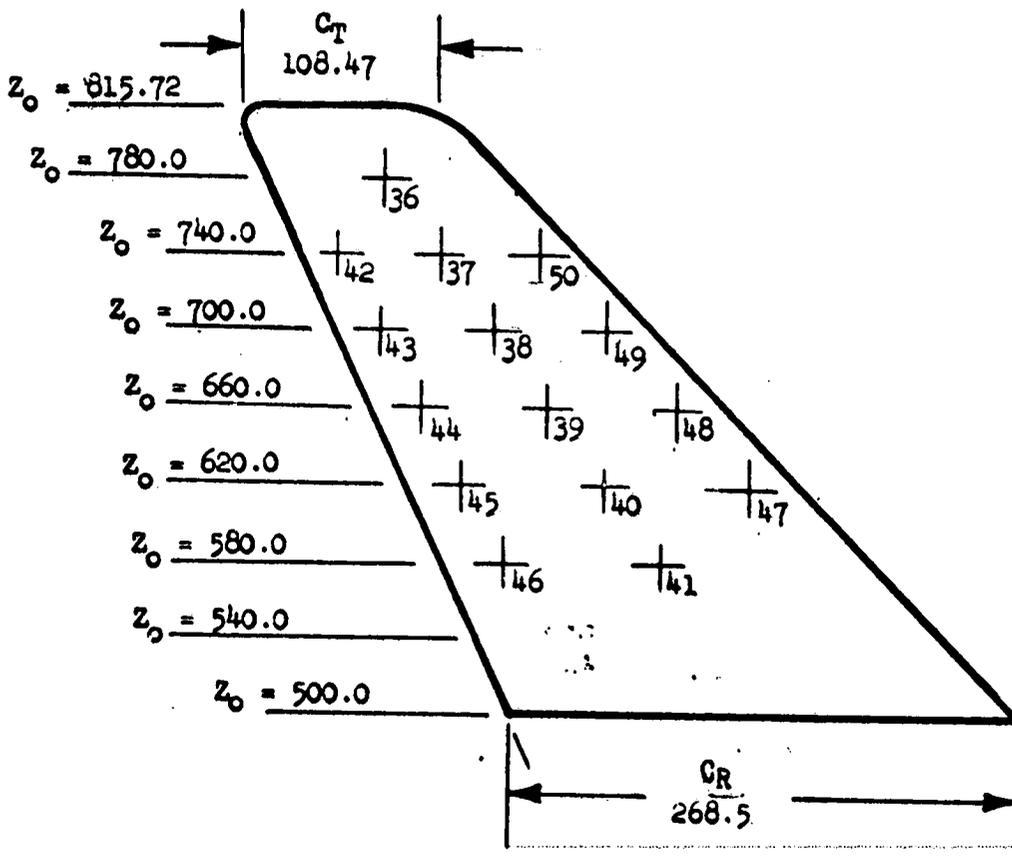
Figure 2. - Continued.

L/H LOWER AFT FUSELAGE PRESSURE TAPS (7)

<u>TAP NO.</u>	<u>X<sub>0</sub></u>	<u>Z<sub>0</sub></u>	<u>LOCATION.</u>
26	1492.0	358.0	L/H LOWER AFT FUSELAGE (BOAT TAIL AREA)
27	1492.0	312.0	
28	1438.0	335.0	
29	1390.0	358.0	
30	1390.0	312.0	
31	1369.0	312.0	
32	1350.0	342.0	L/H LOWER AFT FUSELAGE (BOAT TAIL AREA)

Pressure Tap Locations

Figure 2g. - Concluded.



h. Pressure Taps on the Right Side of the Vertical Stabilizer and Rudder  
Figure 2. - Continued.

VERTICAL TAIL (R/H) PRESSURE TAPS (15)

TAP NO.	X <sub>0</sub>	Y <sub>0</sub>	LOCATION	
50	1533	740	R/H SIDE OF THE VERTICAL TAIL AND RUDDER	
49	1495	700		
48	1460	660		
36	1616	780		
37	1587	740		
38	1557	700		
39	1528	660		
40	1500	620		
41	1471	580		
42	1641	740		
43	1619	700		
44	1596	660		
45	1576	620		
46	1553	580		
47	1423	620		R/H SIDE OF THE VERTICAL TAIL AND RUDDER

Pressure Tap Locations

Figure 2h. - Concluded.

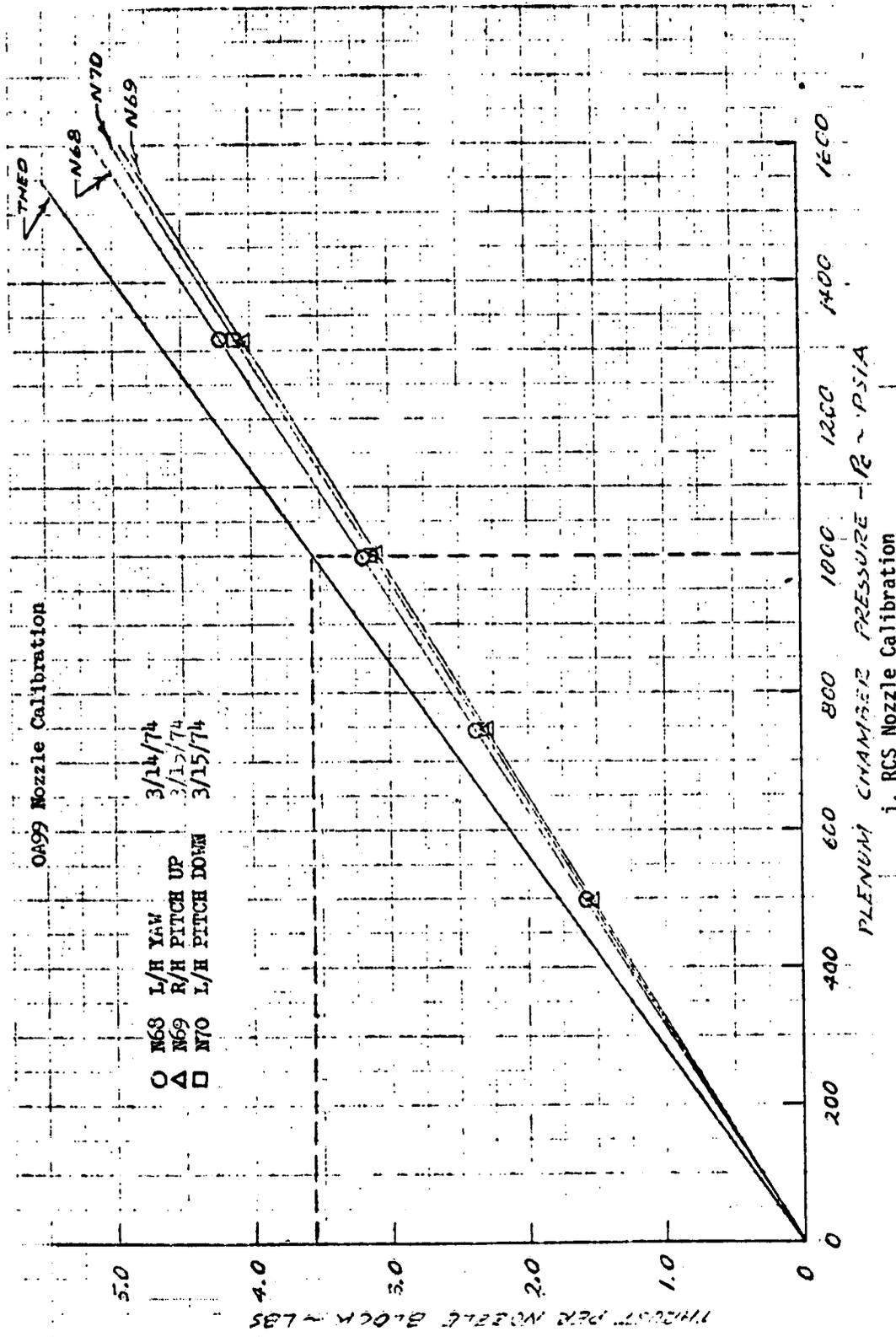
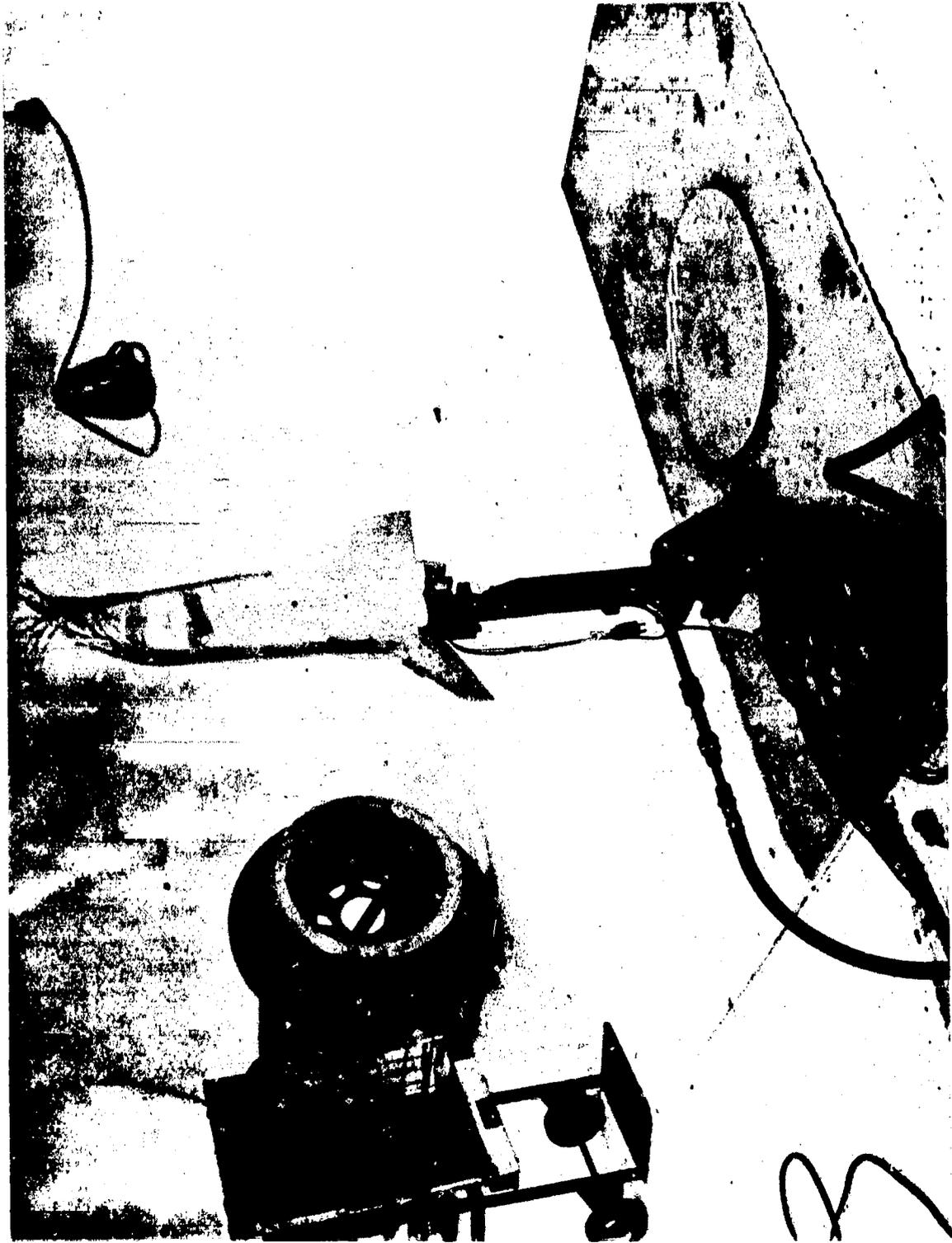


Figure 2. - Concluded.

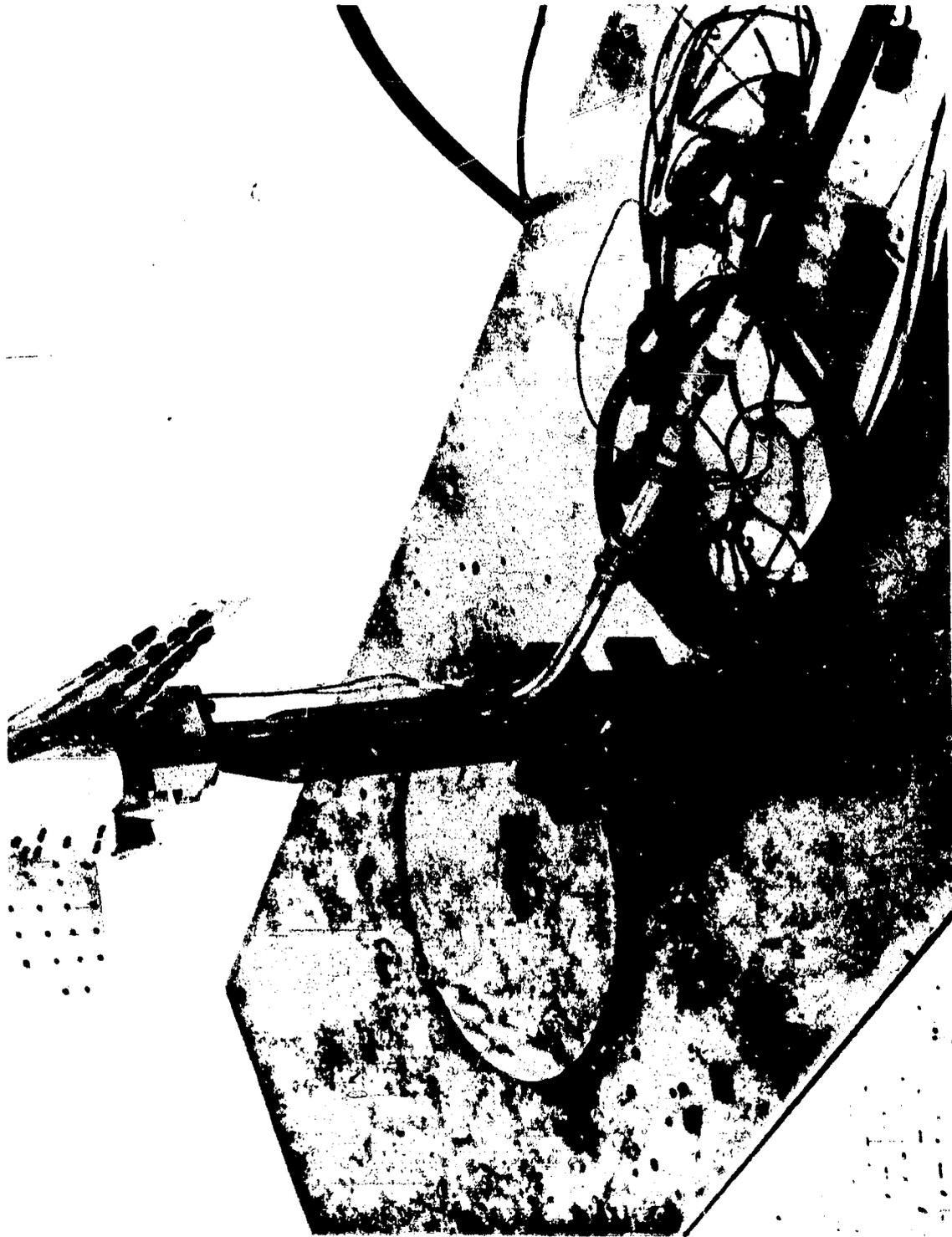
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a. General Installation Photograph

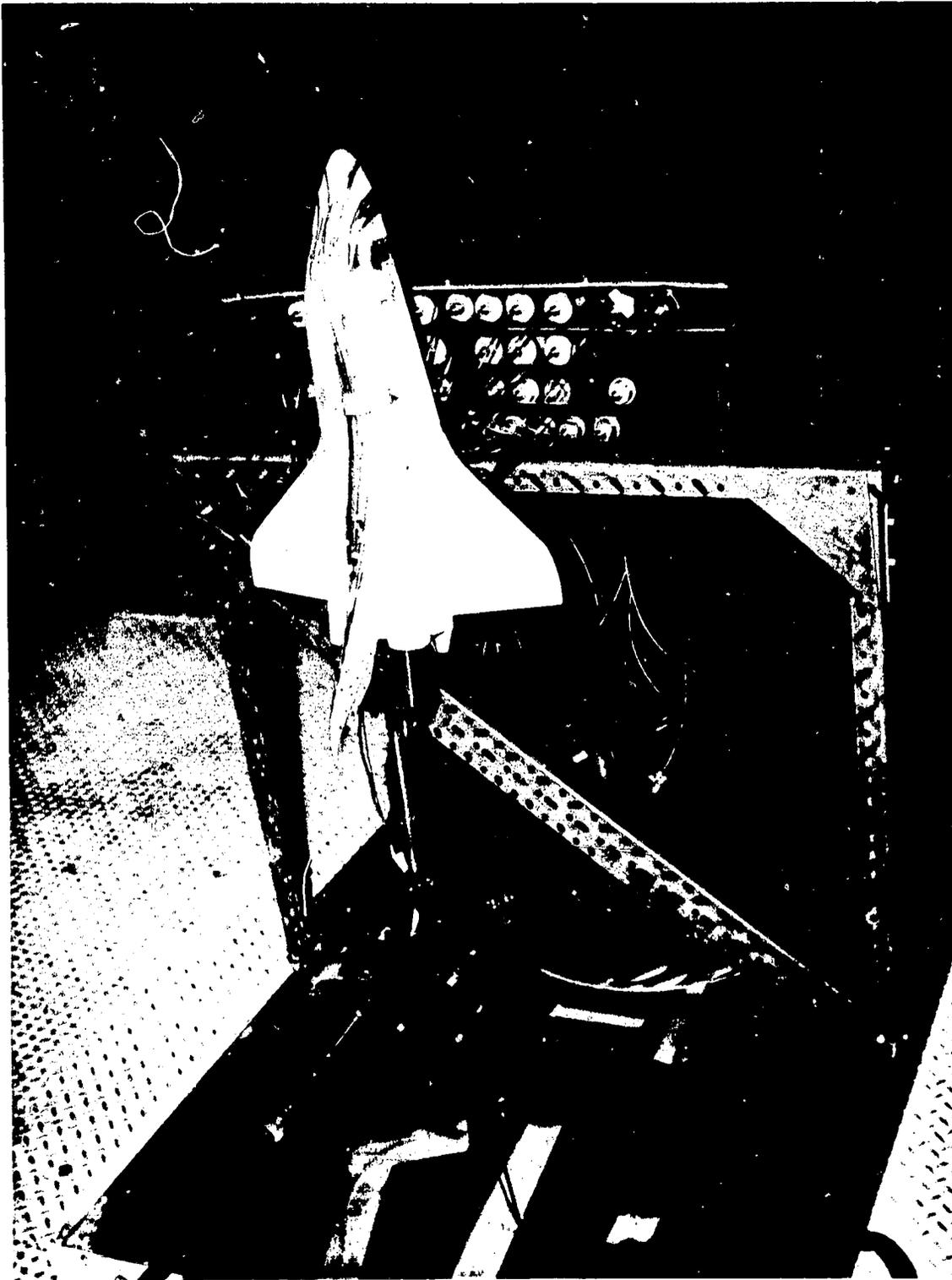
Figure 3. - Model photographs.

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b. RCS Nozzle Block Installation

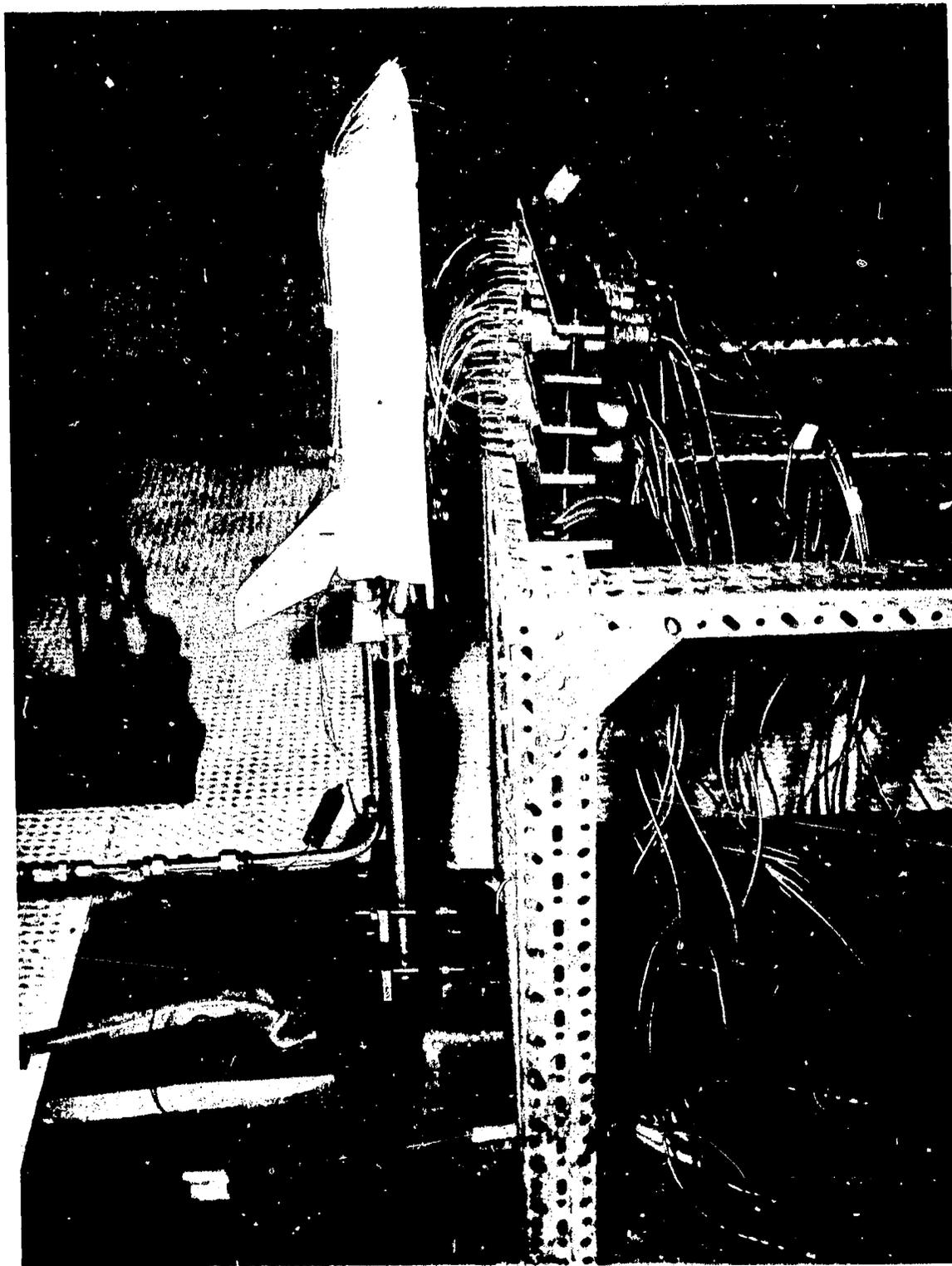
Figure 3. - Continued.



c. Pressure Tap and Transducer Installation Photograph-Plan View

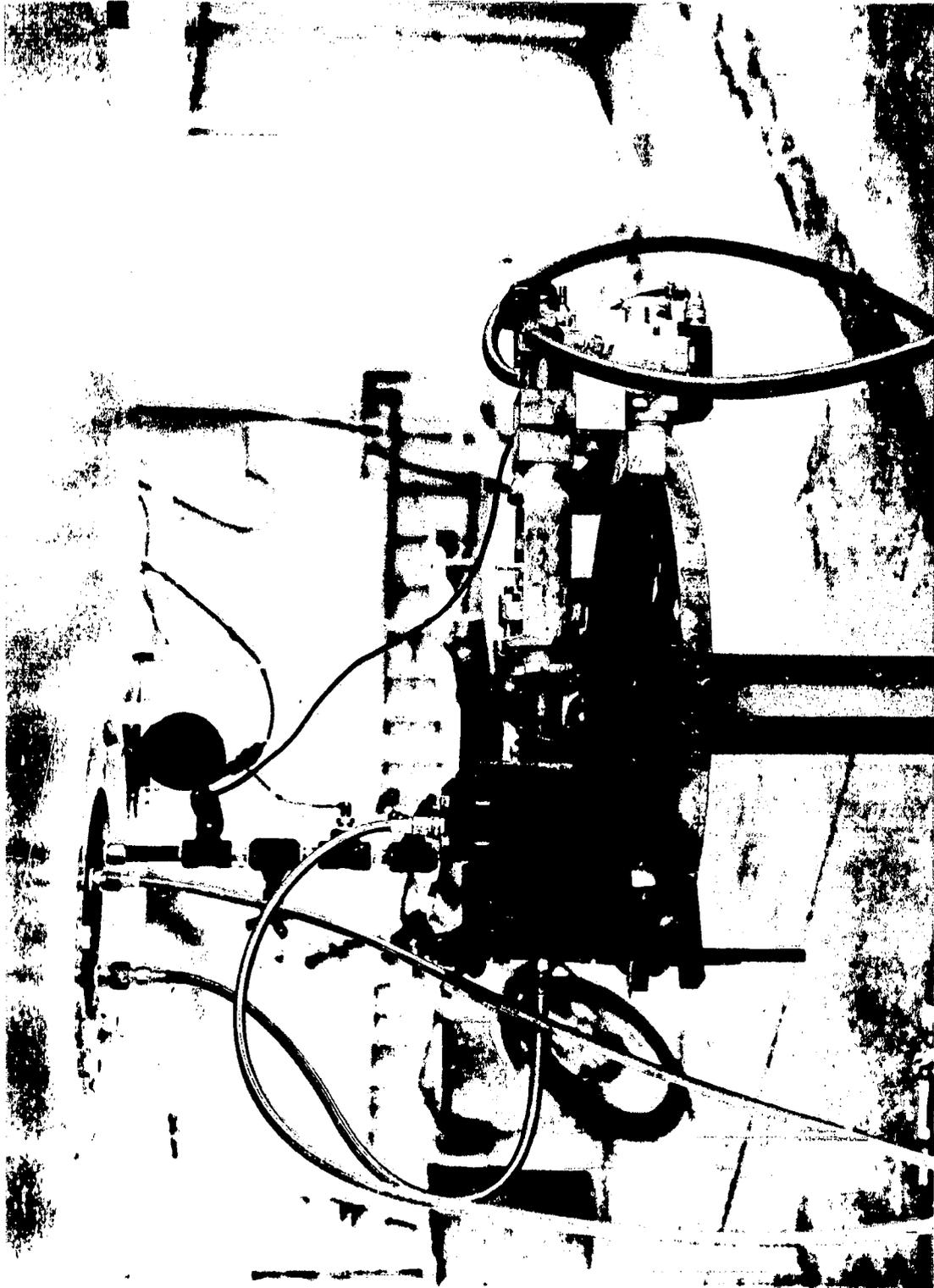
Figure 3. - Continued.

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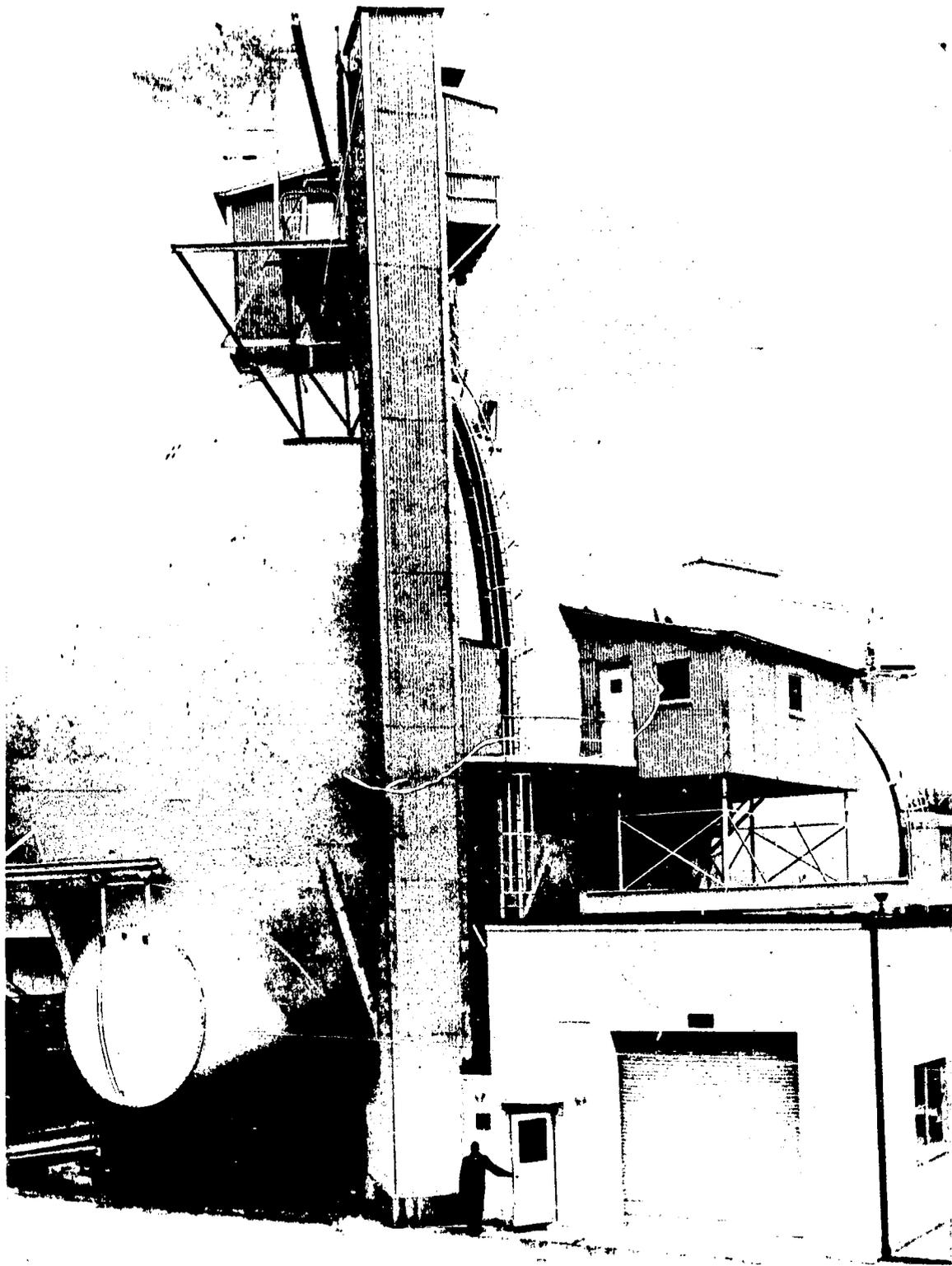


d. Pressure Tap and Transducer Installation Photograph-Side View

Figure 3. - Continued.



e. Hyd. Valve System Installation.  
Figure 3. - Continued.



f. LaRC 60-foot Vacuum Sphere Facility

Figure 3. - Concluded.

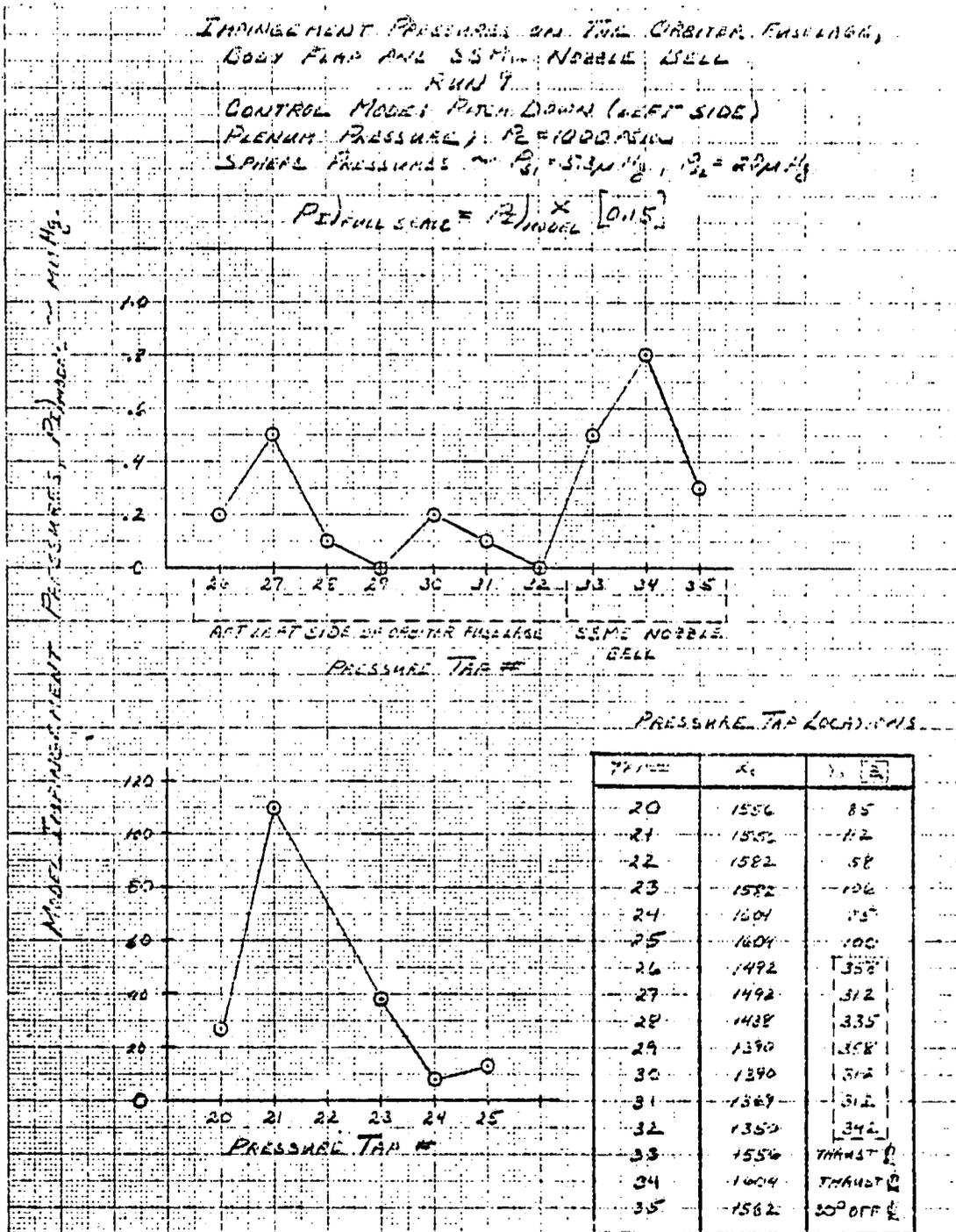


Figure 4. - Impingement Pressures on the Orbiter Fuselage, Body Flap and SSME Nozzle Bell.

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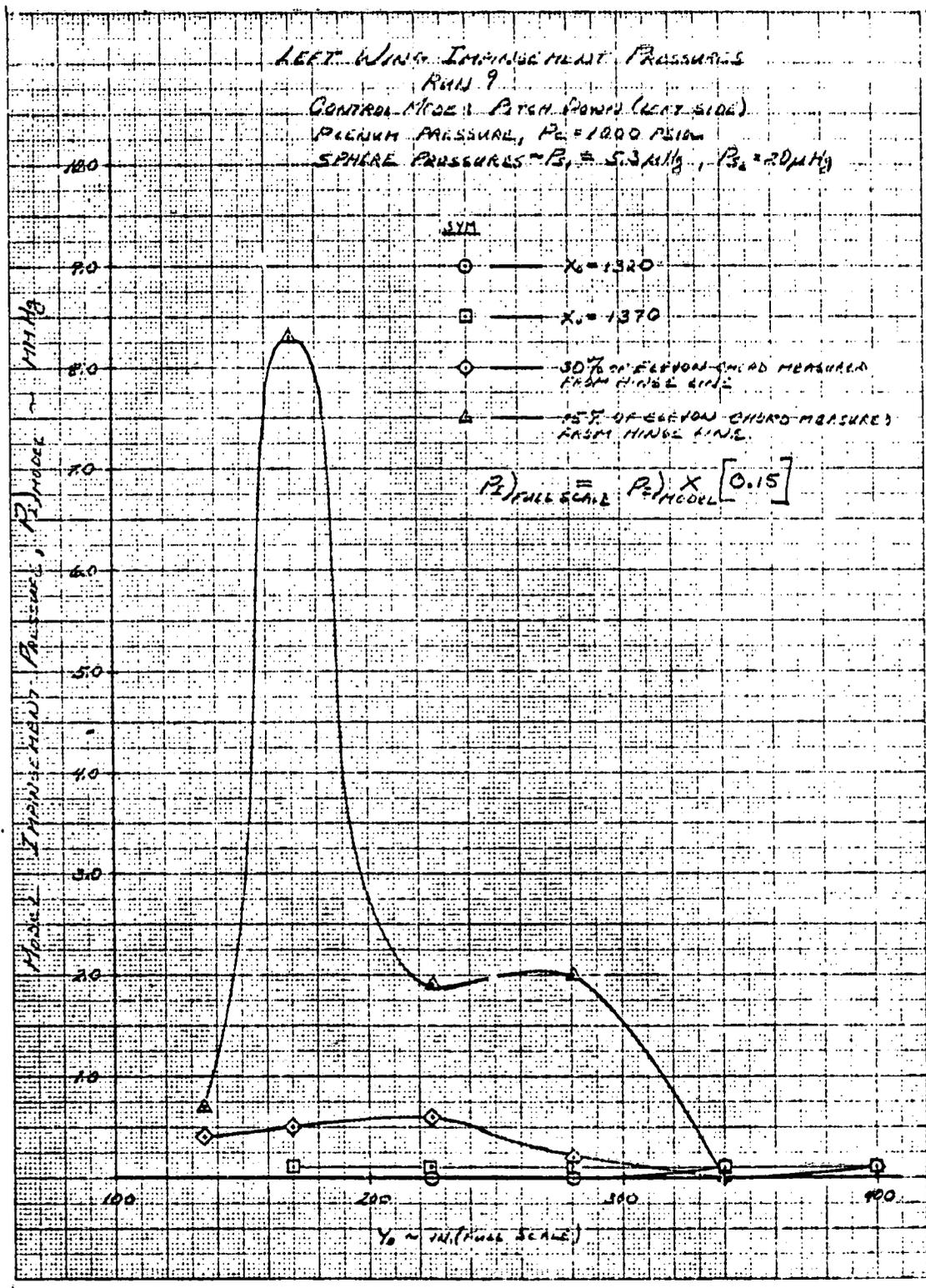


Figure 5. - Left Wing Impingement Pressures.

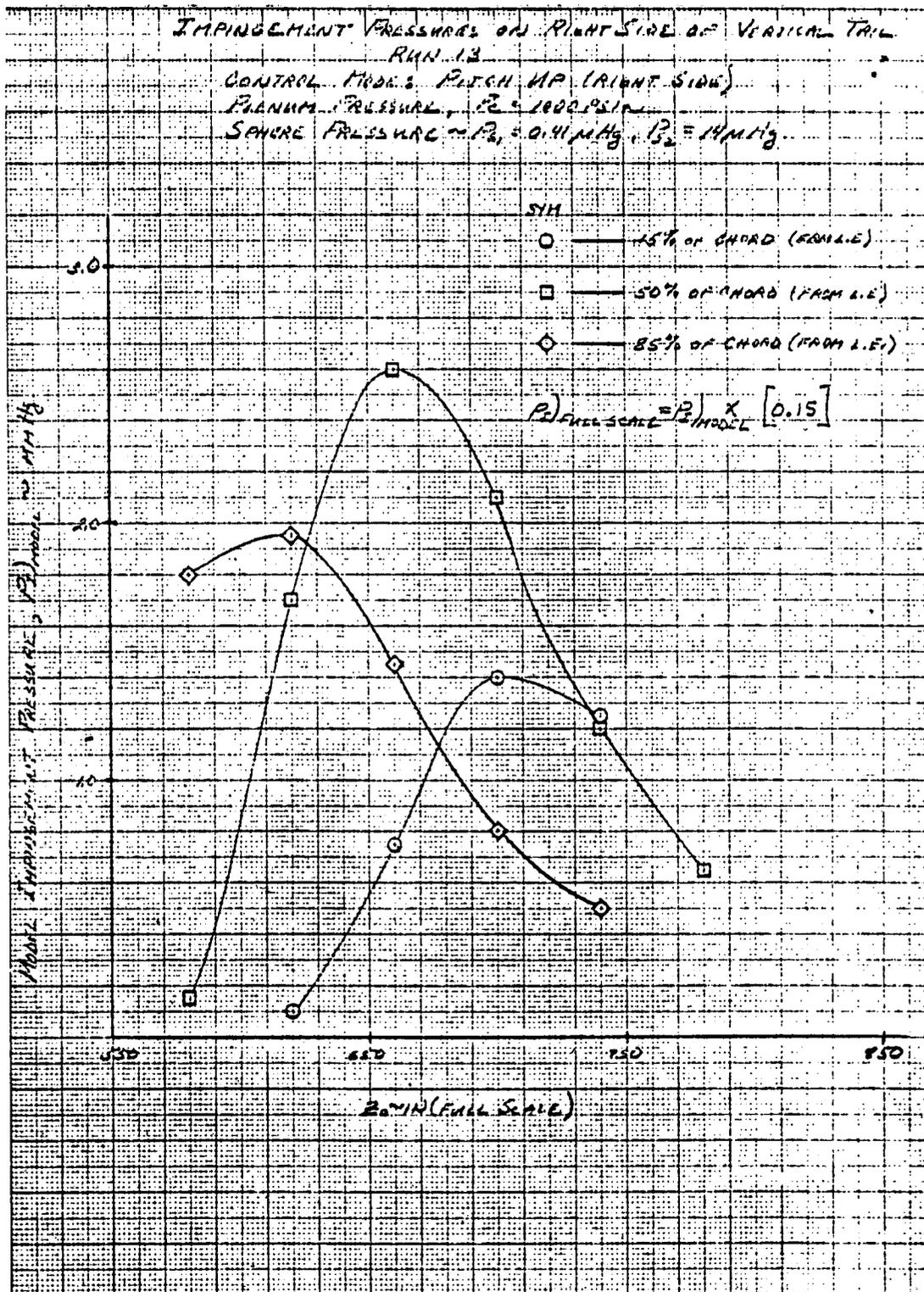


Figure 6. - Impingement Pressures on Right Side of Vertical Tail.